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THE DSN AND TDC NEUTRON TRANSPORT CODES

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THE DSN AND TDC NEUTRON TRANSPORT CODES

by

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ABSTRACT

This report describes two reactor codes, one for the one-dimensional geometries (DSN) and the other for the finite cylindrical case (TDC), based on the transport difference equations and calculation methods developed in <u>Numerical Solution of Transient and Steady State Neutron</u> Transport Problems (LA-2260).

Appendices I and II, which contain the actual machine codes, have been separated from the descriptive part of the report to make it easier for the user to study the material and apply it to problems.

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I. INTRODUCTION

By means of the reactor codes presented here, the DSN and TDC codes, a variety of neutron transport problems may be solved. These codes are written in the language of Floco II¹ for use on the IBM Type 704 calculator, and are based on a modified S_n -approach to the numerical solution of the transport equation.² The DSN code applies to systems described by one space variable, i.e., to systems with infinite plane (slab), infinite cylindrical (rod), or spherical symmetry. In essence it replaces the SNG code,³ but also expands upon that code, since a number of new features have been added in DSN.

The S_n method was reexamined about six months ago, and it was then found that the method could be simplified and generalized, to make it practical to consider multi-dimensional transport calculations. The TDC code represents the first code, based on the new approach, capable of handling more than one variable. It pertains to a two-dimensional

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^{1.} The Floco II Manual, LAMS-2339

^{2.} Numerical Solution of Transient and Steady-State Neutron Transport Problems, LA-2260

^{3.} The S_n Method and the SNG Code, LAMS-2201 (T-1-159).

system, the finite cylinder. To date, TDC calculations have shown every sign of being stable, accurate, and reasonably rapid, competing well in speed - in contrast to SNG and DSN - with the corresponding diffusion calculations. With success in the case of the finite cylinder, it should be a routine matter to write other multi-dimensional transport codes.

With the new S_n difference equations one obtains physically reasonable results even with relatively few intervals, for no restrictions are placed on interval sizes. One can, in fact, use the DSN code to solve infinite medium problems, by using just one very large interval. Normally, we feel, it should be sufficient to use half as many intervals in each variable as one is accustomed to use in diffusion calculations, and fewer than this - for example in parameter studies - if the geometry of the reactor permits it. High-precision calculations will however, as always, require high order S_n calculations with a large number of space intervals. To save time, such calculations should of course be started from results obtained by cruder intervals and a lower n.

The Floco II system is a considerably improved symbolic "load-andgo" coding system, particularly with regard to symbolism, input-output features, and programming control. The DSN and TDC codes handle very extensive problem complexes. It would be impractical to code such problems in either FORTRAN or SAP-type coding systems, unless, of course, one is satisfied with dividing the complexes in many separate codes with fixed limits on the number of materials, space points,

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velocity groups, etc.

Since the Floco II language is simple, brief, and precise, it is not necessary to describe every detail of a code verbally. With respect to DSN and TDC, the user should first familiarize himself with the reports LA-2260 and LAMS-2339 and, second, with the actual codes, Appendix I (of this report) for DSN and Appendix II for TDC, and then examine these codes for details when questions arise. Brief definitive descriptions of the two codes will be given below. In general, a particular problem is defined by a set of input parameters plus a set of functions, some of which require input, and the solution results from executing a collection of coded formulae under control of a master code (the Flow Code, here formula #803).

The DSN code contains about 1800 instructions, the TDC about 2000, and Floco II itself occupies about 2500 memory locations. The codes can therefore be used on 704's with memory capacities of 8192 or more words. Although both codes are by now fairly well checked out, other difficulties may arise in some applications. A few of the numerical methods involved are new and not yet fully understood; in some instances they could possibly fail. The code admits physically questionable input data, e.g., negative scattering cross sections; in such cases no guarantees can be made. For some problems single precision 704 arithmetic is not adequate for the accuracy required, etc. To date, however, we have not encountered, in our own applications, any impossible situations.

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II. THE DSN PARAMETERS

To prepare a DSN calculation, 28 parameters must be specified as follows (for example, see Appendix I):

- <u>AO1</u> The regular (AO1 = 0) or adjoint (AO1 = 1) solution of the transport equation may be specified.
- The problem type may be either inhomogeneous (A02 = 0), or A02 homogeneous (A02 \neq 0) with an "eigenvalue" to be determined. If A02 \neq 0 the reactor must contain fissionable material. <u>A02 = 1</u> implies a reactivity (k) calculation, i.e., DSN is to vary k (which divides the fission density FO) until criticality is achieved. A02 = 2 specifies a type of time-dependent (α) calcula-The neutron flux is assumed separable with respect to the tion. time t and the time variation given by a factor exp (α t). The quantity α enters into the collision term only, σ is replaced by $\sigma + \alpha/v$, where v is the neutron velocity. <u>A02 = 3</u> implies that the concentration (c) of specified isotopes is to be varied. The vector PO is furnished with basic concentrations, P4 with modifiers, and DSN computes the effective concentrations from PO + $c \cdot P4$ (see further $p \cdot 10$). A02 = 4 specifies that the thick nesses of certain material zones are to be varied $(\delta$ -calculations). The interval lengths (D6) given implicity by the input radial points, and the δ -modifiers (D4) listed by zones (numbered 1,2,3,..., and given by interval # in R7), are used to calculate

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the effective intervals (D1): $D1 = D6 (1 + \delta D4)$. If <u>A02 = 5</u>, the whole reactor is to be uniformly expanded or contracted (a-calculations) until criticality is achieved.

- <u>A03</u> The geometry may be either slab (A03 = 0), rod (A03 = 1), or sphere (A03 = 2).
- <u>A04</u> The central (r = 0) boundary condition is specified by A04. For rods and spheres it is assumed always perfectly reflective (A04 = 1). For slabs there are two other options, A04 = 0 signals a free boundary (vacuum to the left) and is used when the slab system is not symmetric about a central plane. A04 = 2, which implies A05 = 2, specifies a periodic condition, i.e., the flow at the center (for each angular direction into the reactor) equals the flow at the outer boundary (for the corresponding outward directions).
- <u>A05</u> The outer (r = a) boundary condition is specified by A05. It may call for zero inward flow (A05 = 0), perfect reflection (A05 = 1), or slab periodicity as defined under A04 (A05 = A04 = 2), now involving those S_n angular rays directed to the left.
- <u>A06</u> The outer (power) iteration count is produced in A06. Initially A06 is set to 0, 1, or 2, to start the count and at the same time specify the input neutron flux. If A06 = 0 or 1, the coder provides a flux as a function of r for N4. If <u>A06 = 0</u>, DSN places N4 in

block NO - where the flux as a function of r (radius) and g (velocity group) is to be located - for g = the base group (GO2) with zeroes in all other NO locations. If <u>AO6 = 1</u>, then K7 • N4 is placed in NO, where K7 is the relative fission spectrum as a function of g. Exceptions: if AO1 = 1 or AO2 = 0, then AO6 = 1 is assumed equivalent to AO6 = 0. If <u>AO6 = 2</u>, then a dump (result from a previous calculation) or other complete input for NO is provided by the coder. This input must have IO4 (no. of intervals) and GO1 (no. of velocity groups) as required by the problem being prepared. If <u>AO6 = -2</u>, then the complete input for NO has IO4 = 1/2 of the IO4 for the problem.

- <u>A07</u> The order of the desired S_n approximation (2,4,6,...) is given in A07. The coder supplies a set of S_n constants (Appendix I) for input into blocks M5, M6, M7. One set is used if A03 = 0 or 2, another if A03 = 1, and the latter is expanded (with input for M4 also) for the TDC code.
- 101 IOl is the problem identification number, a fixed or floating point number.
- 102 IO2 gives the number of material zones in the reactor, a zone being a more or less arbitrary grouping of contiguous intervals. One usually takes a zone to mean a reactor region with uniform material composition, involving a fixed density and isotope

combination.

- <u>IO3</u> Multi-group transport theory with either isotropic (IO3 = 0) or a form of linear anisotropic (IO3 = 1) scattering may be specified. TDC handles the first of these cases only.
- <u>104</u> The total number of space (r) intervals in the system, $i = 1, 2, \dots, 10^4$.
- <u>105</u> 105 gives the first guess for the eigenvalue (k, α , c, δ , or a). Enter zero here and in 106 if A02 = 0. If 105 specifies a, this quantity need not equal the last radial point given; the code adjusts the radii (RL) by the appropriate factor.
- 106 The second eigenvalue guess is given here.
- 107 This parameter specifies $\epsilon(\lambda)$, the precision wanted of the calculation. The precise meaning of ϵ can only be ascertained from experience with many calculations. Here λ is the total neutron population decay factor. If $\lambda < 1$ the system is super-critical, if $\lambda > 1$ the system is sub-critical. A λ is computed for each power iteration (during which the fission density is held fixed) and four successive λ 's are saved. Convergence for a particular eigenvalue (p) is defined by $|\lambda_k - \lambda_{k-1}| < \epsilon(\lambda)$ for all three values of $\lambda_k - \lambda_{k-1}$. Final convergence is defined by $|1 - \lambda_k| < 2\epsilon(\lambda)$ for the four values of $1 - \lambda_k$ available. After

DSN has determined $\lambda(105)$ and $\lambda(106)$, it proceeds to use an interpolated value (corresponding to $\lambda \approx 1$) saving the quantity $dp/d\lambda$ for the further modification of p which may be required before the final convergence criterion is satisfied.

- <u>GO1</u> The number of neutron groups is given by GO1, g = 1, 2, ..., GO1, where g = 1 represents the neutrons of highest energy (lowest lethargy), and g = GO1 the lowest energy group. If AO1 = 1 the cross section matrices in block CO are internally rearranged so that the a regular solution procedure is imitated. In the process the ordering of the groups is reversed by the code.
- <u>GO2</u> The base group GO2 is normally taken to be the group of highest energy with non-zero neutron flux (initially and throughout the calculation), thus if AO1 = 0, GO2 = 1, and if AO1 = 1, GO2 = GO1. Other choices may be made if these particular groups are vacuous or contain but few neutrons. The point of the base group is that the code computes a "distance" (ϵ_k) between successive fluxes (NO^k, NO^{k-1}) for that group, whereupon calculations (one or more "inner" iterations) are performed on the succeeding groups until the equivalent accuracy, at least, has been achieved for these. The base group should therefore be one with a comparatively long neutron mean free path (on the average over the reactor).

GO3, GO4, GO5 specify the form of the cross section matrices, which

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contain one column for each group. Position GO3 in a column contains σ^t , the total transport cross section, with position GO3 - 1 occupied by $\nu \sigma^{f}$, ν times the fission cross section. If GO3 > 2, the positions above GO3 - 1 may be filled by other cross sections of the coder's choice. These are not used by the DSN code except in the preparation of "activities," i.e., cross sections times the final neutron fluxes. The position $\underline{GO4}$ contains σ_{gg}^{S} (self-scattering). The positions GO3 + 1 to GO4 - 1, if any, are filled with speed-up cross sections, position GO4 - 1 with scattering cross sections from the group below (in energy), position GO4 - 2 with similar data for moving neutrons up two steps in energy, etc. GO5 specifies the last position in the column. Positions GO4 + 1 to GO5 are filled with slowing-down cross sections, position GO4 + 1 with data for slowing down by one step, etc. Positions in the matrix with no physical meaning are filled with zeroes. Note also that DSN assumes that if position g', $g' > GO_4$, contains a zero, all succeeding entries are zero. Three additional vectors are regarded as part of the cross section input, the relative fission spectrum (K7), the velocities (V1), and v as a function of g (N7).

GO6, GO7 are used by DSN, but are not input parameters; enter zeroes.

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- <u>MO1</u> The total number of isotopes for which input cross sections (for CO) are provided is specified in MO1. The isotopes are numbered (1,2,...,MO1) in the order loaded. If a material is described as anisotropic in scattering, two matrices are provided, and the subsidiary one is loaded just after the principal one, and numbered accordingly. The subsidiary table contains only speed-up and slowing-down cross sections. In entering MO1 one must then count anisotropic materials twice.
- The total number of isotopes and isotope combinations are specified M02 in MO2. The latter are numbered MO1 + 1, MO1 + 2,..., MO2, with two successive numbers assigned to anisotropic combinations. The composition of mixtures are specified in IO and PO if MO2 > MOL. Thus, if three materials (1,2,3) are involved (MOl = 3) and two mixtures (4,5) are to be formed, #4 from 1 and 3 with densities ρ_1 , ρ_2 , and #5 from 1, 2, and 3 with ρ_3 , ρ_4 , ρ_5 (MO2 = 5); enter 1, 3, -4, 1, 2, 3, -5 in IO and ρ_1 , ρ_2 , O, ρ_3 , ρ_4 , ρ_5 , O in PO (MO3 = 7). The minus sign on material numbers signals mixtures to be formed. If material #2 in this example is anisotropic the basic materials would be 1, 2, 3, 4 (MO1 = 4) the mixtures 5 and 6 (MO2 = 7), and the IO entries 1, 4, -5, 1, 2, 4, -6. In the latter case one must also fill I4, of length MO2, to mark with l's the anisotropic materials; in this example the I4 entries are 0, 1, 0, 0, 0, 1, 0.

- MO3 MO3 specifies the number of entries required in IO (or PO) to define the desired isotope combinations. If MO1 = MO2, then MO3 = 0.
- <u>MO4</u> The order of "smear" is specified in MO4. By smear we mean mixtures of isotopes and isotope combinations, by order of smear, the maximum (over all space intervals) of entries required to specify the material composition in any interval. If no smear is required, i.e., if all intervals can be specified in terms of the materials 1,2,..., MO2, then MO4 = 1. Smears may be used in a variety of situations, e.g., when there is differential loading or burn-out within a zone, or variable interpolation between two cross section sets, due for instance to temperature variation in the reactor, etc.
- <u>M05</u> M05 gives the number of entries required in M3 (material #'s) and R3 (densities) to specify the material composition (smear) in every interval. If M04 = 1 and the material composition is uniform by zone, then M05 = IO2. The vector R3 contains, of course, sets of specifications. The last entry in a set is signaled by giving it a minus sign. So that DSN can find the material definition for a particular interval, the coder provides in S7, by interval #, the position of the first entry of the set in R3 which applies.

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MO6, MO7 are used by DSN, but are not input parameters; enter zeroes.

- <u>SO1</u> The absence (SO1 = 0) or presence (SO1 = 1) of a distributed source QO is specified here.
- SO2, SO3 are not used by DSN; enter zeroes.
- <u>SO4</u> The absence (SO4 = 0) or presence (SO4 \neq 0) of a surface source Q4 at the outer boundary is specified here. If SO4 \neq 0, which implies A05 = 0, then Q4 contains either one vector q_g (SO4 = 1) or two successive vectors q_g , q'_g (SO4 = 2). In the first case an isotropic source is assumed with q_g as input for each negative S_n direction (μ), in the second case (linear source), DSN computes $q_g + |\mu| q'_g$ as the boundary input.
- <u>S05</u>, <u>S06</u> If S05 = 0, no effect, if S05 = 1, the calculation assumes a fixed k given in S06 and A02 may have any value except 1. If S05 = 2, the calculation assumes a fixed α given in S06 with any $A02 \neq 2$.
- S07 S07 is used by DSN, but is not an input parameter; enter zero.

III. THE TDC PARAMETERS

The parameter specifications in TDC, 30 in number, are quite similar to those in DSN.

AO1 See DSN.

- <u>A02</u> See DSN if A02 = 0 and for k, α and c calculations. A02 = 5 is omitted in TDC; it is a special case of A02 = 4. If <u>A02 = 4</u>, then the thicknesses of zones (either cylindrical shells, slices or both) may be varied until criticality is achieved. The effective r-intervals (Dl) are given as in DSN by Dl = D6(1 + δ D4). Similarly, for intervals in the axial variable z (Zl): D2 = D7 (1 + δ D5), where D5 are modifiers by axial zone #'s (Z7). If no input is provided for R7 and Z7, and if D4 and D5 are constant (one entry for each), then R7 and Z7 are set to all 1's by the code, and we have effectively an a-calculation. Special cases here are D4 \neq 0, D5 = 0, or vice versa.
- <u>A03</u> In TDC A03 specifies the boundary condition at the bottom of the cylinder. If the cylinder is symmetric about a central plane perpendicular to the axis, that plane is at the bottom. At the boundary we may then call for zero input (A03 = 0) or perfect reflection (A03 = 1).

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- <u>A04</u> The top boundary condition is specified here. It may call for zero flow in (A04 = 1) or for reflection (A04 = 1, S03 = 1), not perfect reflection here, but one correct as far as the current is concerned. In the future, we may substitute a more proper procedure here.
- A05 Same as A04 but referring to the free (curved) surface of the cylinder. If A05 = 1, S04 = 1 also.
- <u>A06</u>, <u>A07</u> as for DSN, except that, if A06 = -2, then the complete input for NO has IO3 and IO4 = 1/2 of the IO3 and IO4 for the problem. Note also that TDC performs an S₂ calculation (the S₂ constants are always loaded into E4, E5, E6, and E7) during the "discrete" part of the iteration scheme, i.e., up to the point where dp/d λ is first calculated, whereupon a switch is made to the precision specified in A07. The object of this procedure is, of course, the saving of computing time.
- <u>IO1</u>, <u>IO2</u> as for DSN, with the comment that the zone #'s (listed by interval #) are stored in FO, in the last few bits of the words, and are here not to be confused with the r and z zoning (R7, Z7) defined for δ -calculations. To save space in TDC, two blocks besides FO are double-valued. The quantities labeled S7 in DSN are placed in the lower bits of the words in WO, and the material #'s labeled M3 in DSN are similarly placed in NO -

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initially - then merged with R3 by TDC before NO is loaded with the initial flux.

<u>103</u> The total number of intervals in the axial direction, j = 1, 2, ...,103, starting at the bottom of the cylinder.

104-107, GO1-GO7, and MO1-MO7 as in DSN.

- <u>SO1</u> and <u>SO2</u> specify the distributed source; if none, enter zeroes. SO1 gives the number of the first group with non-zero input for QO, and SO2 gives the total number of consecutive groups with source input. If some groups within this range have no source, enter the appropriate number of zeroes as part of QO.
- <u>S03</u> The presence of an isotropic boundary source at the top of the cylinder is specified by S03 = 1 (if none, set S03 = 0). If S03 = 1, then A04 = 0.
- SO4 Same as SO3 for the free boundary. If SO4 = 1, then AO5 = 0.

S05-S07 as for DSN.

IV. THE FORMULA CODES IN DSN

The DSN code contains 36 formulae numbered from 800 to 847, where 800, the Initial Code, and 801, the Assign Code, are executed as soon as loaded, and 802 is the collective label for the remaining, with the Flow Code (#803), connecting the formulae in 802, loaded last. The notation follows the Floco II conventions.

- <u>800</u> Initial Code (IC). In this formula a few parameters are computed: M06, M07, TO1, and S07 (see Appendix I). M07 is the total number of S_n discrete angular directions, M07 = A07 + 1 for slabs and spheres, and $(\frac{1}{2}M07 + 1)^2$ - 1 for cylinders. Some of these directions (one for slabs and spheres, $\frac{1}{2}M07$ for cylinders) do not count as far as the average neutron flux is concerned. The fluxes along these directions are to be regarded as initial values for the integrations in the angular variables. These are then only of consequence in curved geometries. Formula 800 also sets ϵ (A06) stored in P04 to unity, the largest distance possible (see p. 8), and computes a number stored as T04, which is used to produce restart dumps periodically.
- 801 Assign Code (AC). This code assigns memory space to all functions involved in DSN calculations.

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- 805 Initial Neutron Flux (NF) sets up a starting flux in NO, as specified on p. 5 under <u>A06</u>.
- <u>806</u> Adjoint Cross Sections (AX). The formula is executed only if AOl = 1 and AO6 \leq 2, and rearranges the cross sections as discussed on p. 8 under <u>GOl</u>, also reversing the order of the elements in K7 (X_g), N7 (ν_g), and Vl (v_g).
- <u>810</u> Mix Cross Sections (MX). Here the cross sections for materials MO2 + 1, MO2 + 2, etc. are generated, using the input cross sections loaded into CO, the quantities IO and PO which define the mixing, also P4 if a c-calculation is called for, and I4 if anisotropic materials are present.
- <u>811</u> Input Print (IP). The quantities listed are printed off-line if A06 ≤ 2 .
- <u>812</u> Modify Geometry (MG). This formula modifies the radial points (r_i) in δ and a calculations. It also computes $Dl = \Delta_i = r_i - r_{i-1}$ and the midpoint r_i 's, $R2 = \bar{r}_i = \frac{1}{\bar{E}}(r_i + r_{i-1})$, except for spheres (see 813) where V4/R2 replaces \bar{r}_i .
- <u>813</u> Geometric Functions (GF). The volume elements VO and V4 = VO/D1 are computed, VO = D1 (slabs), D1 \cdot R2 (rods), and VO = = D1 $\cdot (r_i^2 + r_i r_{i-1} + r_{i-1}^2)/3$ (spheres), thus omitting a factor 2π for rods and 4π for spheres. In addition, two quantities

 Gl_{im} and $G3_{im}$, terms entering the S difference equations, are precomputed here:

Slabs: Gl = 0 $G3 = | \mu_m | / \Delta_i$ Rods: $Gl = \gamma_m / R_i^2$ $G3 = | \mu_m | / \Delta_i$ Spheres: $Gl = \gamma_m / R_i^2$ $G3 = | \mu_m | / \Delta_i$

where $\mu_{\rm m}$ is in M7, $\gamma_{\rm m}$ in M6, and (for spheres) $\Delta'_{\rm i} = \Delta_{\rm i}$ for m = 1, otherwise $\Delta'_{\rm i} = 2\Delta_{\rm i} V_{\rm i}^4 / (r_{\rm i}^2 + r_{\rm i-1}^2)$. For further details regarding the S_n difference equations, see LA-2260.

- <u>814</u> Form Weights (WS). In this formula the weight function $w_i = |\Sigma_g NO_{ig}| \cdot V4_i$ is computed and stored in WO. These weights are partially established on experience, having been found to aid in the estimation of the eigenvalue λ . In TO2 is stored $\Sigma_i w_i |\Sigma_g NO_{ig}|$. At the end of a power iteration the same quantity (TO3) is computed using the then revised NO values. The ratio TO2/TO3 defines λ .
- 815 Fissions Adjoint (FA). Here, if AOl = 1, the adjoint fission density, given by:

 $FO_i = \sum_g \chi_g NO_{ig}$ is calculated. Division by k (IO5) or k (SO6) is performed if specified (AO2 or SO5 = 1).

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<u>816</u> Fissions Regular (FR). Here, if AOl = 0, the fission density: $FO_i = \Sigma_g \sigma_g^f NO_{ig}$,

is computed and division by k or k_0 performed if indicated. σ_g^f is first obtained as a function of radius, taking the material specifications by i (including smearing) into account.

- <u>817</u> Monitor Print (MP). Monitor output is obtained at this point, the printed monitor line giving POl = A06, PO2 = the count of all inner iterations, PO3 (a spare, in the code = 0), PO4 = $= \epsilon$ (A06), PO5 = IO5, PO6 = dp/d λ , PO7 = the neutron balance indicator (PO7 should ideally equal GOl, the number of groups), and finally PlO = λ . For further details see Appendix I. Switches 1, 2, and 3 come into play in this formula, #3 selects the card reader, if the operator wishes to change some of the input data and then proceed.
- 821 Effective Cross Sections (EX). An array of cross section columns (for a particular g) is formed here, one column for each i, and stored in H2. The material specifications are fully taken into account.
- <u>820</u> Anisotropic Cross Sections (EZ). This formula is executed if IO3 = 1 and a table of σ 's, as in 821, is formed in A2 for the anisotropic components.

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- <u>822</u> Path Lengths (PL). Three positions of block H2, those containing σ^{t} , $v\sigma^{f}$ and σ^{s}_{gg} are selected, and the data transferred to H1, H4, and H5, respectively. Actually $\frac{1}{2}\sigma^{t}$ is placed in H1 and modified, if A02 or S05 = 2, by $\alpha/2v$. A special procedure is used if $\sigma + \alpha/v$ becomes negative (see code).
- 823 Source Term (ST). The source term of the transport equation is calculated for a particular g:

$$SO_{i} = \chi_{g} FO_{i} + \Sigma_{gi} \sigma_{g'g} NO_{ig'} + QO_{ig} \quad (regular)$$
$$SO_{i} = \nu \sigma_{g}^{f} FO_{i} + \Sigma_{g'} \sigma_{g'g} NO_{ig'} \quad (adjoint)$$

with summation (for each i) over the scattering cross sections $\sigma_{g'g}$ in the H2 columns (see 821).

<u>824</u> Source, Anisotropic Part (SZ). The source is in the anisotropic case given by SO_i + $\mu_m S_{i}^{A}$, with $S_{i}^{A} = 3\Sigma_{g}, \sigma_{g'g} J_{ig'}^{O}$

where $\sigma_{g'g}$ here are the anisotropic components of scattering stored in A2 (see 820).

<u>825</u> Boundary Conditions (BC). This formula executes the specification in A04, A05, and S04, for each μ_m and each group. Since, in reflective or periodic situations, NO at $\mu = 0$ and the outer boundary is given theoretically by S0/2HL, the input flux is given, for arbitrary μ_m , in terms of (S0/2HL)(1 + Bl_{mg}), where Bl_{mg} is reestimated at the end of each iteration on a particular group. Bl_{mg} is, in other words, obtained by an iteration concurrent with the regular one. We do not know as yet whether this procedure always gives proper convergence or not.

- <u>826</u> Perpendicular Flux (PF). This formula computes for fixed g the angular flux along the initializing μ -directions, of significance in the curved geometries.
- <u>827</u> Angular Flux (AF). This formula calculates the angular flux for fixed g along the basic S_n directions μ_m defined in LA-2260. These fluxes are averaged over m (but not in 827) to obtain the total flux NO, and with weights μ_m to obtain the net current JO. If any integration step here or in 826 yields a negative flux, the calculation is repeated using the alternate difference equations as discussed in LA-2260. The integration steps are performed from the outside of the reactor inward, if μ_m is negative, otherwise in the direction of increasing r.
- 831 Current (JC). The current JO is computed in this formula for a particular g.
- <u>830</u> Boundary Values (BV). The quantities Bl_{mg} , if required by the conditions specified, are revised here (initially $\operatorname{Bl}_{mg} \equiv 0$):

$$Bl_{mg}$$
 (rev.) = $(O_m - I_m)/3(O_m + I_m) + Bl_{mg}$

where O_m and I_m are the appropriate outward and inward angular fluxes along the directions μ_m and $-\mu_m$, respectively. The above formula is essentially an empirical one, which so far has proved satisfactory.

- <u>833</u> Boundary Flow (BF). Here the currents, inward and outward separately, are computed at both r = 0 and r = a.
- <u>834</u> Neutron Balance (NB). In 834 a summary is performed yielding the NB factor J03: J03 = (leakage + collisions)/sources. This factor should ideally be unity in a precise calculation. Care is taken at both r = 0 and a to count negative leakage as source so that the scaling process in 835 will work.
- 835 Scaling (SC). The scaling process defined in LA-2260 is performed here, the final result being a scaled average flux NO for a particular g, which is temporarily stored in N⁴.
- <u>836</u> Inner Iterations (II). In 836 N4 is first transferred to its proper place in NO and the data displaced there moved to N4. The distance ϵ is then computed:

$$\epsilon = (\Sigma_{i} | N_{i}^{4} - N_{i}^{0} | w_{i}^{0})/TO2$$

except for the first inner iteration, in which case NO is

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multiplied by λ . If g = GO2, the base group, ϵ is normally sent to PO4, otherwise ϵ is compared with PO4 and if $\epsilon >$ PO4 another iteration on the same group is performed, first modifying SO:

$$SO_i$$
 (rev.) = $SO_i + \sigma_{gg}(NO_{ig} - N4_i)$

For various controls on the inner iteration procedure, see code.

- 837 Group Print (GP). This is a monitor on the results after the completion of a particular group iteration. A line is printed offline if an error indicator has been set, or on-line if Switch # 1 is down regardless of indicators. The line contains JOL = group #, JO2 = scale factor, JO3 = NB factor, JO4 = leakage, JO5 = collisions, JO6 = source, JO7 = error indicators (lst set), and JLO = error indicators (2nd set). Both JO7 and JLO may be logical sums of indicator settings. Indicator JO7 is built up by 1 if the inner iteration count is large (set in 836), by 2 if FO is negative, etc. (Appendix, p. 3).
- <u>840</u> Interpolate (IN). In this formula new parameters (eigenvalues) are obtained by interpolation, which, of course, may amount to extrapolation in some cases. Care is taken to prevent unreasonable values, which may come about due, for instance, to poor initial guesses. If the "interpolated" parameter lies outside one of two limits computed using the initial guesses IO5 and IO6, one of these limits becomes the new IO5, and IO6 is taken to be either the previous IO5 or IO6, depending on which one is closest

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to the new I05, and the iterative procedure is continued. Once the interpolate value is "in range," $dp/d\lambda$ is computed, and from then on I05 is calculated (in 847) from I05 (new) = $(1-\lambda)dp/d\lambda$ + I05.

- <u>841</u> Weights and Test (WT). This formula performs calculations as in 814 (WS). In addition, it includes the shift of the λ -set, the computation of the new λ , the convergence test for the current eigenvalue, and, if AO2 \neq 0, a scaling of NO to make total fissions sum up to unity.
- <u>846</u> Final Print (FP). At the end of the calculation the quantities listed in 834 are printed. There is also in DSN a "forced convergence" technique, for the purpose of terminating a calculation, for whatever reason, which is brought into play by depressing Switch #4.
- <u>847</u> New Parameters (NP). This formula is activated if the convergence test in 841 is satisfied, it controls the various procedures for calculating new parameters, and includes the final convergence test.
- 803 Flow Code (FC). The Flow Code controls the whole DSN calculation, the first action it takes is to print the storage map, using the Floco II subroutine #976.

845, 842, 843, 844 (SM, SS, SK, SL). Summary Formulae. See Section VI.

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V. THE FORMULA CODES IN TDC

The TDC code contains 39 formulae numbered from 800 to 847, where 800, the Initial Code, and 801, the Assign Code, are executed as loaded, and where 802 is the collective label for the remaining, with the Flow Code (#803), loaded last, connecting the other formulae in The whole TDC code is organized in a manner quite similar to 802. The integrations are performed starting with the top slice of DSN. the cylinder and each slice is treated as in the DSN cylindrical case, except that there is, of course, neutron flow in at the top surface, and flow out at the bottom (of each slice). When the bottom slice has been reached and the integrations performed here, the bottom boundary conditions are applied, and the process just described is repeated, now going from the bottom of the cylinder to the top, with neutron flow in at the bottom of each slice and flow out at the top. Thus, in total there are twice as many integration directions in TDC as in the DSN cylindrical case, and the TDC time of calculation is then approximately equal to 2J (2103) multiplied by the time for a DSN rod calculation with the same number of r-intervals. For more details regarding the formulae listed below see either Appendix II or Section IV.

800 Initial Code (IC). Similar to 800 in DSN; the masks needed for the double storage in FO, WO, and R3 are computed here.

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- 801 Assign Code (AC).
- 804 Merging (RN). The material #'s loaded into NO are placed in R3 merged with the R3 input.
- 805 Initial Neutron Flux (NF).
- 806 Adjoint Cross Sections (AX).
- 810 Mix Cross Sections (MX).
- <u>807</u> Exchange S_n Constants (EN). The S_n constants are exchanged twice during a calculation: at the beginning of the calculation to place the S_2 constants in M4, M5, M6, and M7, and after dp/d λ has been formed to place the S_n constants, n = A07, in those blocks.
- <u>811</u> Input Print (IP). The quantities listed are printed if AO6 \leq 2.
- <u>812</u> Modify Geometry (MG). This formula handles the modification of r_i and z_j as needed in δ -calculations, computes Δ_i (D1), Δ_j (D2), and V_i (V0), $V_i = \frac{1}{2} \Delta_i (r_i + r_{i-1})$.
- <u>813</u> Geometric Function (GF). Here the quantities Gl, G3, and G5, terms entering the S_n difference equations are precomputed:

 $Gl = \gamma_m/R2_i, G3 = |\mu_m|/\Delta_i, G5 = \bar{\mu}_m/\Delta_j,$ where μ_m (M7), γ_m (M6), and $\bar{\mu}_m$ (M4) are S_n constants.

814 Form Weights (WS).

- 820 Vertical Current (VC). This formula is used when the next current is required at either the top or bottom of the cylinder. The current as a function of r is placed in J⁴ and the integrated current in FO⁴.
- 816 Fissions Regular (FR).
- 815 Fissions Adjoint (FA).
- 817 Monitor Print (MP).
- 821 Effective Cross Sections (EX). Here as in DSN the table H2 of cross sections is formed for a fixed g; but for a particular j only.
- 822 Path Lengths (PL).
- 825 Boundary Condition (BC). This formula handles the conditions at the curved boundary.
- 823 Source Term (ST).
- 824 Top Boundary (TB). This formula handles the conditions at the top boundary of the cylinder. Also, a number of blocks are cleared: N4 in which the new neutron flux is to be accumulated, J5 and J6 where the horizontal inward and outward net currents (functions of j) are to be accumulated, and L0, L1, L2, and L3 where certain sums are formed for the neutron balance and scaling calculations.

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- 826 Perpendicular Flux (PF).
- 827 Angular Flux (AF).
- 830 Horizontal Current (HC). Here the currents at the free boundary are calculated (for fixed j), separately for inward and outward directions.
- 831 Bottom Boundary (BB). The formula handles the conditions at the bottom boundary of the cylinder.
- <u>833</u> Top Boundary Flow (TF). The boundary values $T5_{im}$ are computed in 823, to be used in setting a reflective condition, at the top, for each i, if A04 = 1.
- 832 Free Boundary Flow (FF). The boundary values F5_{jm} are computed here, to be used as in 833, but for the free boundary. Also, the quantities needed for the scaling and the final neutron balance, for the current value of g, are computed here and cumulated.
- 834 Neutron Balance (NB).
- 835 Scaling (SC).
- 836 Inner Iterations (II).
- 837 Group Print (GP).
- 845, 842, 843, 844 (SM, SS, SK, SL). Summary formulae. See Section VI. 840, 841, 846, 847, 803, (IN, WT, FP, NP, FC). See DSN.

VI. ARRANGEMENT OF THE DSN AND TDC DECKS

The DSN and TDC decks are arranged in the same manner. The cards are loaded in the order in which they are described.

1. <u>Floco-2 deck</u>. This deck is completely self-contained: it is self-loading and contains its own transition card.

2. <u>Parameter header</u>. This card initializes loading and storage assignment addresses.

3. <u>Parameter cards</u>. A00 is normally loaded first. If a punch dump is to be loaded, the first four cards following the punch ID are loaded after the initial parameters; these four cards must be preceded by a 9* A00 card.

4. <u>IC header</u>. This card reserves storage for formula sets 800, 801, and 802; it also sets NLA to the proper value to load formula 800.

5. Formula 800.

6. Transition card for formula 800. Formula 800 is executed.

7. AC header. This card sets NLA to load formula 801.

8. Formula 801.

9. Transition card for formula 801. Formula 801 is executed.

10. <u>Remark cards</u>. Formulas 850 to 863 are loaded here. Formula 850 may be changed from problem to problem to provide an identification on the listing.

11. <u>General code header</u>. This card sets NLA to load the 802 formula set.

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12. Formulas 804 to 847.

13. Formula 803. This is the Flow Code.

14. <u>Data</u>. If a punch dump is being loaded, the NO cards must be preceded by a 9×10 card. If Bl cards are dumped, these must be identified (by comparing the loading address with the storage map) and preceded by a $9 \times Bl$ card. In TDC, the cards for R3 and NO must be followed by an I* 4804 card.

15. <u>Transition card for 803.</u> This card starts the problem running.

<u>Use of Switches</u>. Switch #1 is placed in the down position if additional monitor printing is desired, e.g., the group monitor (see 817 and 837). If Switch #2 is depressed a restart card dump is obtained (see 817); on pressing "Start," the calculation is resumed. Switch #4 is used to force convergence, i.e., to terminate the problem arbitrarily with a final print and a restart dump (see 837 and 846).

<u>Summary</u>. At the end of a calculation a summary of "activities," average cross sections times neutron fluxes, is generated by zone, where data for zone #0 (the whole reactor) are first given. Two tables, A and B, are printed for each zone:

Table A contains columns corresponding to the entries in the cross section tables, up to and including entry #GO3, followed by two columns, one for entry #GO4 (self-scattering) and the other for the total scattering cross section, and then by two final columns, one for the

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neutron flux and the other for the source QO, if any. The entries in a particular column give the activity by velocity group, the last entry being the total for all groups.

Table B is arranged as Table A, except that the last two columns are omitted, and the activity is given by material number rather than by velocity group.

LAMS-2346, Appendix I PHYSICS AND MATHEMATICS TID-4500, 15th Ed.

LOS ALAMOS SCIENTIFIC LABORATORY OF THE UNIVERSITY OF CALIFORNIA LOS ALAMOS NEW MEXICO

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THE DSN CODE

by

B. Carlson C. Lee J. Worlton

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UNIVERSITY OF CALIFORNIA

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IN REPLY REFER TO:

July 6, 1960

To: Copyholders of LAMS-2346, Appendix I

From: Report Library

Please staple the attached revision pages to the inside front cover of LAMS-2346, Appendix I.

Changes in the DSN Code, I LAMS-2346, Appendix I

1) The " ϵ -system" in the DSN code has in some instances failed to bring about convergence to a principal eigenvalue. The code changes given under Revision I (attached) defines a different and more satisfactory procedure. The ϵ given in IO7 assumes now a different meaning; it specifies the accuracy wanted in the solution of the difference equations for each neutron group, holding the eigenvalue (IO5) fixed. The variable ϵ (PO4) is set to 10^2 IO7 whenever iterative calculations begin on a new fixed IO5 and PO4 is then allowed to decrease as the calculation progresses until PO4 < IO7, and the λ (PLO) last found is taken as the λ corresponding to IO5. <u>Note</u>: Until experience in choosing ϵ is available take ϵ =10⁻⁴/no.

of groups.

2) The empirical procedure for imposing a reflective (or periodic) condition at the outer boundary has proved to be unsatisfactory as was expected. A proper procedure has now been established. It involves keeping the reflected neutrons fixed (except for a scale factor) during a given outer iteration. The code changes are given under Revision II (attached).

Note: The corresponding corrections should be made in TDC if difficulities in these areas are encountered.

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