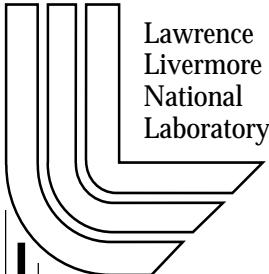


Array Experiments (Phase 1) Volume 1 (with Deletions)

September 2002 (date of release)

U.S. Department of Energy



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Table of Contents

	<u>Page</u>
Detailed description of proposed studies (8/4/64)	4
Report of trip to LASL	16
Misc. program notes	20
Information on elemental impurity analyses	25
Concepts for accident calculations	27
Analytical information - Phase I parts	29
Inspection and evaluation information - Phase I parts.	29
Storage rack safety study	32
Assembly table counter calibrations	41
Study of self-multiplications and temperatures	47
Nuclear safety study with un-moderated parts	49
Assembly: A-1	49
A-2	49
A-3	50
A-4	51
A-5	52
A-6	53
A-7	54
A-8	55
A-9	55
A-10	56
A-11	57
A-12	57
A-13	58
A-14	59
A-15	60

Assembly: A-16	
A-17	
A-18	
A-19	
A-20	

<u>Page</u>	
61	
62	
63	
64	
66	

Study of bare 8 member quasi-cubic array 67

Assembly: B-1	67
B-2	68
B-3	69
B-4	70
B-5	72
B-6	74
B-7 (Took to critical)	76
B-8	80
B-9	81
B-10 (Took to critical)	83

Summary data plots on bare 2^3 array 88

Conference with R. Hugley and E. Hill from USAEC-SAN²⁰

on 8/30/64.

Purpose of this meeting was for the AEC people to find out what our intentions were in assay area. (They had been shown our proposal memo., COPP-64-28, by A. Blader, who has begun procedures for obtaining allocation of the plutonium.)

Their interests were generally: Hugley - materials allocation and Hill - operational safety.

I described our plans in the light of the description beginning on page 4.

I told them that we regard this program as a weapons related program, which, we understood, was exempt from the formal hazards analysis requirements of reactor-oriented programs.

They recommended that we perform a minimal study to evaluate the credible accident:

- 1) If the yield is within the scope of the Bldg 110 hazards summary report, prepare a statement to that effect; or
- 2) if the yield exceeds the scope of the existing hazards summary report, prepare an addendum to the Bldg 110 hazards summary report to cover the assay experiments.

A. Williams went to Hanford 7/31/64 to discuss procurement of the array units.

Their current position is that "weapons grade" Pu is in short supply currently ($Pu^{240} \approx 6\%$). They suggested that if we could use "unclassified" Pu ($Pu^{240} > 6\%$) the procurement problems might be greatly eased. The product which would be available would be ~~the~~ $7\frac{1}{2} - 8\frac{1}{2}\% Pu^{240}$. From operational viewpoint this should be satisfactory; however, must evaluate from Oscar Kolar's viewpoint.

The proposed unit for the array is a 3 kg cylinder, $2.59''(2\frac{19}{32})$ I.D. There would be ≈ 5 mils clearance laterally. This would permit pretty accurate indexing of locations of the Pu part. The can would be sealed in the usual manner, cleaned of removable L-contamination and painted with acrylic paint.

Latest estimate on price and availability is a change from previous time:

- 1) \$30,000 cost of processing
- 2) Availability: 90 days after release of material. (Need clarification: full delivery in 90 days or partial delivery earlier?)

8/11/64

O. Kolar agreed that the "unclassified" Pu would be adequate for our needs for the simple arrays. Informed May Harris of this decision.

Discussed the program support generalities with Dick Adelmann. Still is considerable uncertainty about what division will sponsor this program; Dick suggested that the various key figures concerned should have to work this out.

9/23/64

Conference with Z. Zandtner, W. Miller, M. Harris, O. Kolar, A. Williams. 22

What are cost requirements?

What magnitude of cost for Pu units?

Custom can should cost ~ \$2,000

- 1) Cost estimate for Hanford proposal.
- 2) Cost estimate for custom can approach.

Getting Pu material.

- 1) Off-spec availability not good; hence will require an order for "weapons quality" material.

Nov 6 1964

Comparison between Lab BF_3 and Westinghouse BF_3

Source - PuBe MRC-52 $> 10^6 \text{n/sec}$

#1 Chambers 3" away from source

Lab. Spade Beckman BF_3

6.5×10^{-13}

Lab. BF_3

8×10^{-13}

Westinghouse BF_3

1.2×10^{-10}

#2 Chambers $23\frac{1}{4}$ " away from source

Lab BF_3 8×10^{-14}

Westinghouse BF_3 1.2×10^{-11}

Westinghouse more sensitive than Lab BF_3 by a factor of 150 with a PuBe source energy spectrum

Louis Sherman
Arnold Reyenga

11/24/64

Array unit storage racks. The storage racks are designed to provide a minimum of 8 inch center-to-center spacing for storage of array units. The framework is shown in LRL Drawings #

~~64~~

64-119656

64-119637

64-119623

64-119597

In addition each unit will be contained in a watertight box with a gasketed lid held on with snap fasteners.

Misc. Information 1/18/65

Project responsibilities: DMA Ofc. Project Officer: F. Fairbrother

W-Div Project Manager: Don Gath 8202

Account Numbers: Personnel Time 5110-65

All procurement 5110-85

Accountability requirements for billets (per O. Mezdors)

Need way to check wt. of each unit:

1. Tare wt. for can
2. Net wt. of Pu

Need individual unit number reasonably permanently attached.

Also need total Pu and net Pu^{239}

Based upon Williams trip to Hanford 1/15/65, we should expect the following:

1. Chemical analysis of all billets (see next pages)
2. Isotopic analysis of every 5th billet.
3. Density variation within 19.40 - 19.60 g/cc.

Because of insufficient wheelbase in dollies on machine it was decided to build new assembly machine instead of using current one. Overall extent for array structure set at 7 ft on each edge of a cube.

Will also get a weighed (~5g) sample of same lot of material as billet #1 for use in determining self-multiplications in total immersion counter.

GENERAL  ELECTRIC
COMPANY

RICHLAND, WASHINGTON . . . TELEPHONE Whitehall 2-1111
Extension: 2-7504

**HANFORD ATOMIC
PRODUCTS OPERATION**

**CHEMICAL PROCESSING
DEPARTMENT**
234-5 Bldg., 200-W Area

December 31, 1964

Mr. M. E. Harris 7101
University of California
Lawrence Radiation Laboratories
Building 102, Room 2458
P. O. Box 808
Livermore California

Dear Mr. Harris:

PLUTONIUM ANALYSIS

The following information is forwarded in response to your telephone inquiry concerning analyses performed at Hanford on plutonium. The following elements are analyzed routinely by emission spectrograph methods:

ELEMENTS	LOWER DETECTION LIMIT (ppm)	ELEMENT	LOWER DETECTION LIMIT (ppm)
Al	5	Mn	5
As	20	Mo	10
B	1	Ni	5
Be	1	P	100
Bi	5	K	5
Ca	5	Si	20
Cd	20	Ag	1
Cr	2	Na	2
Cu	1	Ti	20
Ge	2	Sm	2
Fe	50	Tl	2
Pb	2	V	50
Li	1	Zn	20
Mg	2		

Received S.M.S.
JAN 4 1965
ROUTE TO DATE
Harris

RETURN TO SMS
FILE IN
DESTROY

(cont. next page)

Mr. M. E. Harris

-2-

December 31, 1964

The method used in film reading at this location is visual comparison of film densities to standard lines. Readings are therefore accurate within a factor of two except for iron which, by virtue of applying densitometric procedures, is precise to $\pm 20\%$.

Details of our emission spectograph methods are outlined in HW-53368, "Analytical Technical Manual, Chemical Processing Department, Hanford Atomic Products Operation". It is up to date except for the fact that the cupferron procedure for determining Al, Ca, Be, and Ti has been replaced with a sodium-fluoride carrier technique similar to the gallium-carrier technique. Our engineering Files records indicate that two copies were sent to LRL. You may want to inquire in typical places at LRL to locate a copy and refer to it.

Another document which you may want to examine is HW-68159, Revision 1, "Plutonium Product Specifications Analyses". Copy 6-A was forwarded to Dr. M. D. Martin. This document describes briefly analyses that are performed on plutonium metal at Hanford. You will note that analytical procedures other than those we have discussed are presented.

If you require additional information, we shall be happy to try to provide it.


J. V. Brecke
Manager
Weapons Fabrication Operation

LI Brecke:RAZ:jdw

Accident situations for Hazards Review

1. Magnitude of accident with 2% reactivity step increase.
2. Startup accident - I :
 - a. Lattice spacing for 64 - 6 kg units is 0.5 cm less than critical value. (error # 1)
 - b. Period channel fails to provide scram (error # 2)
 - c. Scram occurs on power channels at 3×10^{-9} amp (0.5 watt).
 - d. Closure speed for final 3 inches is 1 in./min.
 - e. Max. response time for scram 5 sec
 - (1) Max. for meter 5 sec (Meter response time $2.3 t$)
 - (2) Circuit response 0.06 sec.
 - (3) Table motion sec
 - f. Source level $6 \times 3.84 \times 10^5 = 2.3 \times 10^7$ n/sec
 - g. Closure continues until scram occurs (error # 3)
 - h. Overshoot depends upon instantaneous period at time scram initiates.
3. Startup accident - II :
 - a. All conditions of 2. are applicable except c.
 - b. Scram occurs on power channels which are erroneously set on their least sensitive ranges - 3×10^{-7} (50 watt) (errors # 4 and # 5).

1/22/64

Further examination of RC circuit characteristics shows that in range of 0.1 to 5 sec periods, the Beckman meter response time goes as $2.3 \times$ Period. Total time

when table begins to move will then be $2.3 t + 0.06$ sec.
Various calculated values are then :

t_{sec}	$t_{resp} (sec)$
0.1	0.3
0.5	1.2
1.0	2.4
5.0	11.5

3/5/65

Had meeting with Special Material Staff: Harris and Bladen, Williams, and a man from ALCO Materials Staff about plutonium procurement.

We derived a schedule which we believed would be workable from our viewpoint:

<u>Assy. Machine</u>	<u>Array</u>	<u># Units</u>	<u>Total Kg. Pu</u>	<u>Date Required</u>	<u>Increment of Pu Mass</u>
Small	2^3	8	24	5/1/65	27 (+some spares)
Large	3^3	27	81	8/1	63
"	4^3	64	192	10/1	114
"	5^3	125	375	12/1	187

Man from ALCO thought that first two dates could be met; latter would ~~probably~~ come in smaller increments. All material would be weapons grade, not high Pu^{240} . This is not a firm commitment, of course.

WEAPONS MANUFACTURING SECTION
ANALYTICAL LABORATORY REPORT

6-10-65

Customer: Lawrence Radiation Laboratory
SANL-235000

Material: Plutonium Metal

Spectrographic Analysis - parts per million parts plutonium

Serial No.	Ag	Al	As	B	Be	Bi	Ca	Cd	Cr	Cu	Fe	Ge	K	Li	Mg	Mn
LRL-001	L1	L2	--	L2	--	--	2	--	L1	L5	L25	--	2	--	5	5
002	L1	L2	--	L2	--	--	500	--	20	L5	L25	--	2	--	5	10
003	L1	2	--	L2	--	--	10	--	1	L5	L25	--	2	--	5	20
004	L1	2	--	L2	--	--	20	--	50	5	L25	--	2	--	5	10
005	L1	2	--	L2	--	--	50	--	20	L5	L25	--	2	--	10	20
006	L1	L2	--	L2	--	--	2	--	L1	5	L25	--	2	--	10	5
007	L1	2	--	L2	--	--	5	--	L1	L5	L25	--	2	--	5	5
008	L1	L2	--	L2	--	--	L2	--	2	L5	L25	--	10	--	5	10
009	L1	L2	--	L2	--	--	5	--	L1	L5	L25	--	2	--	L2	2

Serial No.	Mo	Na	Ni	P	Pb	Si	Sn	Ti	Tl	V	Zn	Percent**		
												TMI*	Purity	
LRL-001	--	2	20	--	L1	L15	2	L2	--	--	--	92	80	99.98
002	--	1	100	--	L1	L15	2	L2	--	--	--	693	100	99.92
003	--	5	20	--	L1	L15	2	L2	--	--	--	118	130	99.98
004	--	L1	100	--	L1	L15	2	L2	--	--	--	143	120	99.97
005	--	2	20	--	L1	L15	2	L2	--	--	--	179	110	99.97
006	--	2	20	--	L1	L15	2	L2	--	--	--	97	70	99.98
007	--	50	20	--	L1	L15	2	L2	--	--	--	143	80	99.98
008	--	10	20	--	L1	16	2	L2	--	--	--	115	95	99.98
009	--	20	L1	--	L1	L15	2	2	--	--	--	88	120	99.98

* Total Metallic Impurities

** 100% - Σ (TMI + carbon)

Receiving Inspection of Pu Slugs - Phase I

Identifying Marks	Contamination Status	Container Condition	Tare = 27.0 g	Slug Wt.	Tare Wt.	Net Pu Wt.
				kg	kg	kg
1. LRL-001-3026	N.D.	OK	tare weighed with wts.		3.026	
2. LRL-002-3036	N.D.	FAIR wimples in edge of can bottoms	"	Tare	27.0 g	3.037
3. LRL-003-3032	N.D.	OK	"		27.0 g	3.043
4. LRL-004-3019	N.D.	OK	"			3.020
5. LRL-005-3004	ND	OK	"			3.004
6. LRL 006-3029	N.D.	OK	"			3.029
7. LRL 007-3013	ND	OK	"			3.013
8. LRL 008-3020	ND	OK	"			3.021
9. LRL-009-3030	N.D.	OK	tare weighed with wts.		3.032	
10 HS-001	-	-			9.620 g	

Remarks:

Billet temp.: 94°F
 Room temp.: 66°F Ave. Billet Wt., kg = 3.025

Standard Deviation, kg = .012
 = 0.4%

WEAPONS MANUFACTURING SECTION
ANALYTICAL LABORATORY REPORT

6/10/65

Page -2-

*Uncertainty
not known*

Isotopic Analysis - weight percent

Serial No.	Mass Spectrometer			Neutron Counter			<u>Net Weight</u>	<u>Plutonium</u>
	Pu 239	Pu 240	Pu 241	Pu 242	Pu 240	n.s.		
LRL-001	93.675	5.871	59.9	0.440	0.014	0.2	5.93	60.5
002	93.579	5.978	61.0	0.425	0.018	0.3	5.96	60.8
003	93.539	5.968	60.9	0.477	0.016	0.3	5.98	61.0
004	93.702	5.837	59.6	0.447	0.014	0.2	5.82	59.4
005	93.782	5.759	58.9	0.445	0.014	0.2	5.80	59.2
006	93.643	5.894	60.1	0.450	0.013	0.2	5.90	60.2
007	93.700	5.844	59.6	0.442	0.014	0.2	5.80	59.2
008	93.639	5.894	60.1	0.453	0.014	0.2	5.88	60.0
009	93.656	5.887	60.1	0.445	0.012	0.2	5.91	60.3

Ave 60.0

Ave 60.1

* Calculated n.s. based on Pu²⁴⁰ only

Approved:

R.J. Johnson

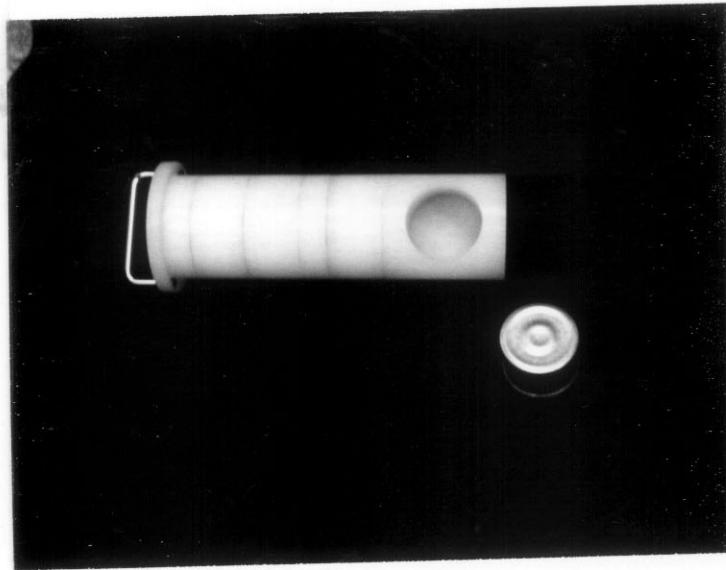
(These numbers from
HANFORD)

By p 715 ANL 5800 Pu²⁴⁰ is $1.01 \pm 0.02 \times 10^3$ n/g sec; Pu²⁴² is 1.7×10^3 n/g sec, Pu²³⁹ 3×10^{-2}

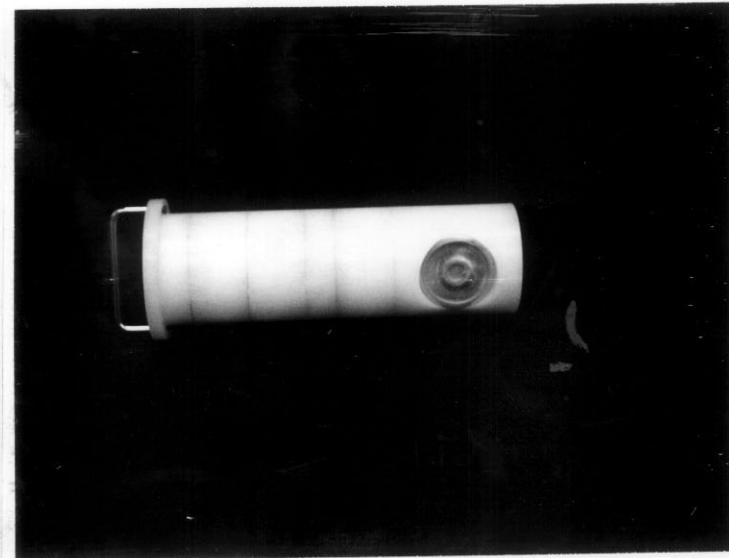
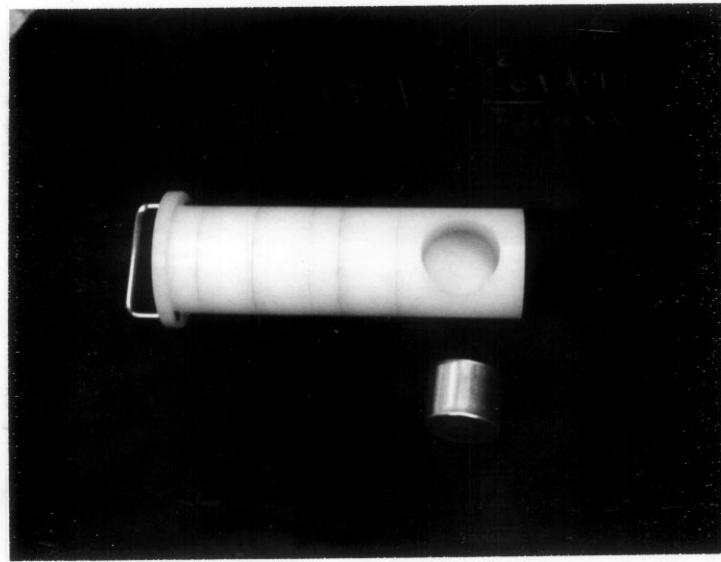
Determination of Neutron Emission Rates

30

Photographs of Slug, Sample Holder, and Counter Setup:



P-38



BG.

$$\frac{314}{627} \text{ c/mm} = 13.7 \text{ c/mm}$$

Ball

$$1282.1 \text{ c/mm}$$

$$\text{Ball - BG} = 1268.4 \text{ c/mm}$$

~~$$\text{eff} = \frac{2.25 \times 10^3}{1.2684 \times 10^3} = 1.77 \text{ Wrong g/cm}$$~~

~~$$\text{Conversion factor} = \frac{2.41 \times 10^3}{1.2684 \times 10^3} = 1.90$$~~

Wt. of historical sample 9.620 grams.

7-7-65

BG. 17.4 c/mm

$$\text{Ball } 32,459 \text{ c/25.2 mm} = 1288 \text{ c/mm}$$

$$\text{Ball - BG} = 1270.5 \text{ c/mm}$$

Sample

$$26126 \text{ c/75 mm} \quad 357.9 \text{ c/mm}$$
$$- BG = 340.5 \text{ c}$$

~~$$\text{Conv. factor} = \frac{2.25 \times 10^3}{1.2705 \times 10^3} = 1.77 = \frac{2.41 \times 10^3}{1.2705 \times 10^3} = 1.90$$~~

$$\frac{340.5 \times 1.77}{9.62} = 67.1 \cancel{62.7} \text{ ngs}$$

Emission Rates (cont.)

Room. Temp.: 66°F

Billet Temp: 94°F ($\Delta T = 28^{\circ}\text{F}$)

Sample	e/m	Bkg e/m	Net e/m	$n/\text{sec} = c/m \times \frac{1.77 \times 10^{-5}}{m}$	N (n/sec)	no (n/gsec)	m no kg	Sample mass kg	Base Rate (= $\frac{Ms}{N \cdot m_{no}}$)
009	{ 102847 297217	130	e/m	4.00×10^5	7.58×10^5	66.9	3.032	2.028×10^5	3.74
004	{ 99922 98567			3.97×10^5	7.52×10^5	65.9	3.020	1.990×10^5	3.78
007	{ 99538 94200			3.87×10^5	7.33×10^5	65.7	3.013	1.980×10^5	3.70
002	{ 103206 100368			4.07×10^5	7.70×10^5	67.4	3.037	2.047×10^5	3.76
001	{ 101278 96623			3.96×10^5	7.50×10^5	67.1	3.026	2.030×10^5	3.69
005	{ 97844 95075			3.86×10^5	7.31×10^5	65.7	3.004	1.974×10^5	3.70
006	{ 101118 98640			4.00×10^5	7.58×10^5	66.8	3.029	2.023×10^5	3.75
008	{ 101559 98387			4.00×10^5	7.58×10^5	66.5	3.021	2.009×10^5	3.77
003	{ 104016 100377			4.09×10^5	7.75×10^5	67.6	3.043	2.057×10^5	3.77

HS001 { 12981 } ^{75mm} 17 340 644 67.1 9.620g ($\leq 1\%$ for this value)
 { 13145 }

From Hanford data and Pu^{240} emission rate of $1.02 \pm 0.02 \times 10^5$ ngs we calculate
 should be 60.5;

* All normalized to fit part 1 and HS1

Average $N = 7.53 \times 10^5$; S.D. of $N = 0.15 \times 10^5$; Average $\frac{N}{m} = 2.49 \times 10^5$; S.D. of $\frac{N}{m} = 5\%$
 (2.0%)

$$\text{Source P-11} = 1.42 \times 10^7 \text{ n/sec}$$

$$\text{Source M-252} = 7.51 \times 10^6 \text{ n/sec}$$

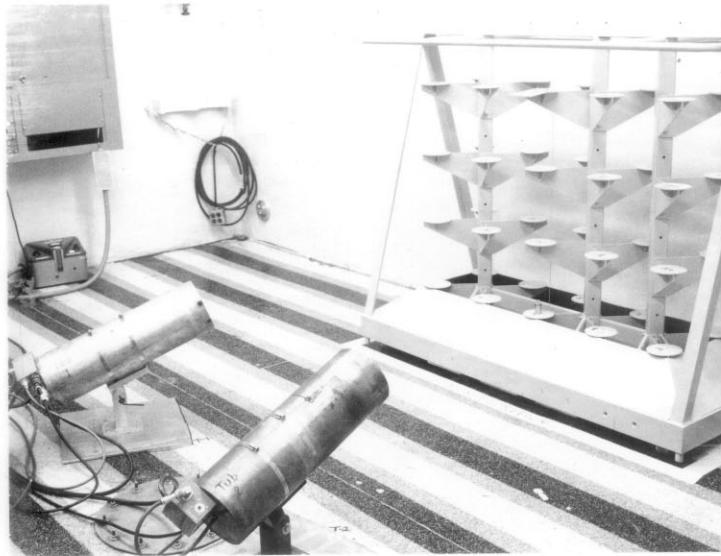
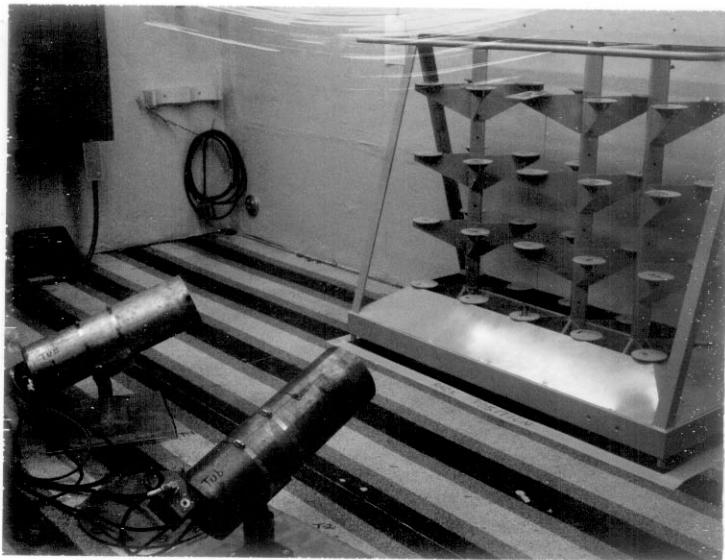
6-22-65

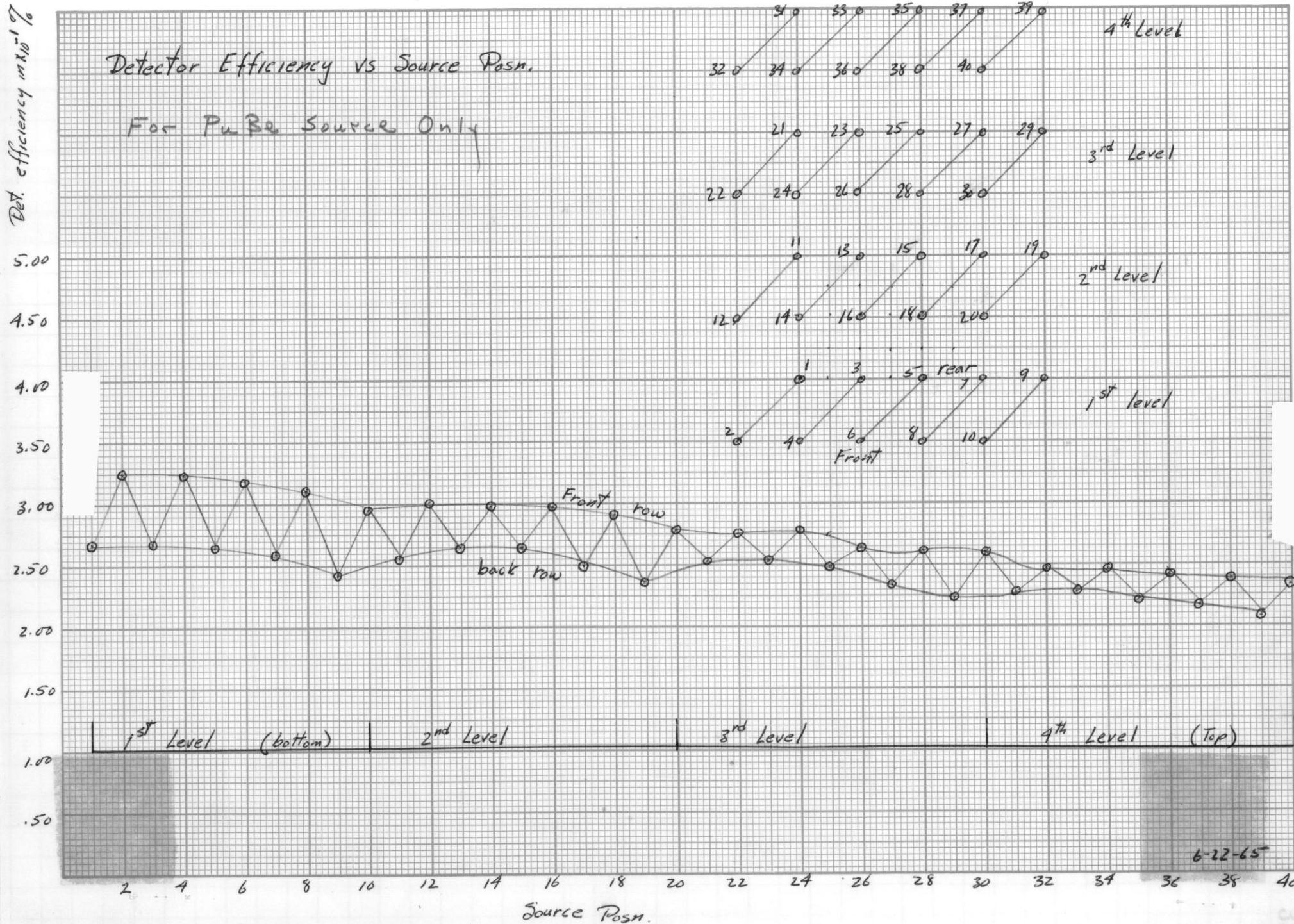
DATA IN THIS TABLE VALID ONLY

FOR PuBe Source Spectrum

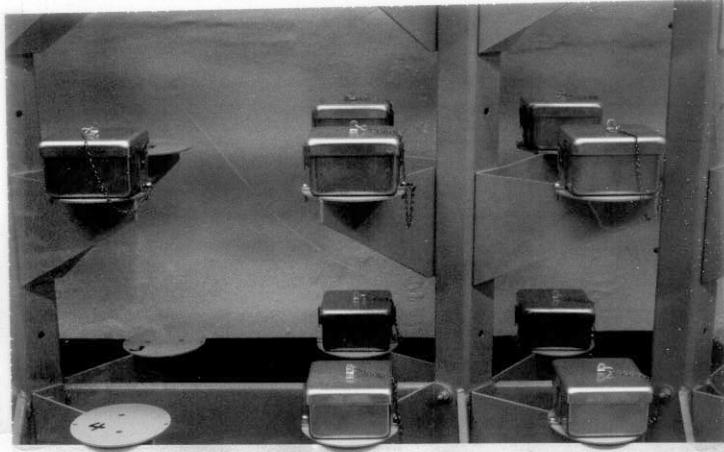
Source Posn	Tub 1	Tub 2	Total	Eff $\times 10^{-3}$
1	20839 /min	17192 /min	38031	2.68
2	25972	20226	46198	3.25
3	19110	18878	37988	2.68
4	23374	22586	45960	3.24
5	17749	19886	37635	2.65
6	21302	23846	45148	3.18
7	16152	20766	36918	2.60
8	18884	25275	44159	3.11
9	13253	21123	34376	2.92
10	16188	25444	41932	2.95
11	19351	16996	36347	2.56
12	23440	19313	42753	3.01
13	18698	18969	37667	2.65
14	21506	20889	42395	2.99
15	18062	19588	37650	2.65
16	{ 19775 19782 }	{ 22390 22242 }	{ 42165 42024 }	2.97
17	16105	19185	35290	2.49
18	18153	23193	41346	2.91

Source Posm	Tub 1	Tub 2	Total	$E\text{ff} \times 10^{-3}$
19	13397	20099	33496	2.36
20	16008	23544	39552	2.79
21	19578	16401	35979	2.53
22	$\begin{cases} 20980 \\ 21049 \end{cases}$	$\begin{cases} 17745 \\ 18213 \end{cases}$	$\begin{cases} 38725 \\ 39262 \end{cases}$	$\begin{cases} 2.75 \\ 2.53 \end{cases}$
23	17714	18154	35868	2.53
24	19636	19866	39502	2.78
25	17115	18249	35364	2.49
26	17786	19680	37466	2.64
27	13981	19180	33161	2.34
28	16669	20508	37177	2.62
29	12362	19355	31717	2.23
30	15537	21582	37119	2.61
31	17574	14833	32407	2.28
32	18642	16424	35066	2.47
33	16104	16444	32548	2.29
34	17705	17323	35028	2.47
35	15258	16183	31441	2.21
36	16108	18274	34382	2.42
37	13269	17612	30881	2.17
38	15229	18616	33845	2.38
39	11638	17936	29574	2.08
40	$\begin{cases} 13965 \\ 14078 \end{cases}$	$\begin{cases} 19070 \\ 19098 \end{cases}$	$\begin{cases} 33035 \\ 33176 \end{cases}$	$\begin{cases} 2.34 \\ 2.34 \end{cases}$





CC
Billet Posn For Phase 1



Increase base rates by 1.11

7/7/65 34

Counting Multiplications in Storage Rack

Part #	Position	cts	Δt	c/m	c/s	M
--------	----------	-----	------------	-----	-----	---

003	5	13453 15064}	20	1425	23.7	
-----	---	-----------------	----	------	------	--

mt 3.043 key ngs 61.0

$$\text{base rate} = 1.85 \times 10^5 \text{ d/s} \times 2.65 \times 10^{-3} = 4.90 \times 10^2 = 490 \text{ c/s}$$

008	7	12345 14668}	10	2702	45.0	
-----	---	-----------------	----	------	------	--

mt 3.021 ngs 59.2

$$\text{base rate} = 1.79 \times 10^5 \text{ d/s} \times 2.65 \times 10^{-3} = 465 \text{ c/s}$$

Since the above numbers are ridiculously low there is obviously some problem somewhere. Array parts put away.

1. Check efficiency factors again with PuBe sources P-11 and M-252 for position #26. Checked out exactly the same for these sources.
2. Since PuBe sources have quite a bit faster neutron spectra than a nominal fission distribution check efficiency factor for position #26 with Pu plug ball

7/8/65

Plug	26	4670	100,	8.50	0.142
ball		5870			

Plug	-	55	60	2.04 (Pu not in entry to A Cell today)
ball		67		

Efficiency factor for #26 for this spectrum is then

$$\frac{1.42 \times 10^{-5}}{2.41 \times 10^{-3}} = 5.90 \times 10^{-5} \text{ or}$$

$$\frac{6.31 \times 10^{-5}}{2.64 \times 10^{-3}} = 2.56 \times 10^{-2} \text{ of efficiency factor for PuBe source}$$

Check Proportionality of Eff. Factors for both
Pu spectrum and PuBe source spectrum:

$$\frac{1}{26} : \frac{6.18}{6.31} = 0.979 \quad \frac{2.68}{2.64} = 1.02 \quad \frac{6.18}{2.68} = 2.30$$

$$\frac{2}{26} : \frac{7.50}{6.31} = 1.19 \quad \frac{3.25}{2.64} = 1.23 \quad \frac{7.50}{3.25} = 2.30$$

$$\frac{3^9}{26} : \frac{5.03}{6.31} = 0.797 \quad \frac{2.08}{2.64} = 0.788 \quad \frac{5.03}{2.08} = 2.42 \quad \left. \right\} \text{top level}$$

$$\frac{40}{26} : \frac{5.51}{6.31} = 0.873 \quad \frac{2.34}{2.64} = 0.886 \quad \frac{5.51}{2.34} = 2.36$$

$$\frac{25^-}{26} : \frac{5.73}{6.31} = 0.908 \quad \frac{2.49}{2.64} = 0.943 \quad \frac{5.73}{2.49} = 2.30$$

$$\frac{3}{26} : \frac{6.18}{6.31} = 0.979 \quad \frac{2.68}{2.64} = 1.02 \quad \frac{6.18}{2.68} = 2.30$$

$$\frac{5^-}{26} : \frac{6.10}{6.31} = 0.967 \quad \frac{2.65}{2.64} = 1.00 \quad \frac{6.10}{2.65} = 2.30$$

$$\frac{6}{26} : \frac{7.31}{6.31} = 1.16 \quad \frac{3.18}{2.64} = 1.20 \quad \frac{7.31}{3.18} = 2.30$$

$$\frac{7}{26} : \frac{6.02}{6.31} = 0.954 \quad \frac{2.60}{2.64} = 0.985 \quad \frac{6.02}{2.60} = 2.32$$

$$\frac{8}{26} : \frac{7.20}{6.31} = 1.14 \quad \frac{3.11}{2.64} = 1.18 \quad \frac{7.20}{3.11} = 2.32$$

$$\frac{26}{26} : \frac{6.26}{6.31} = 0.992 \quad \frac{2.64}{2.64} = 1.0000 \quad \frac{6.26}{2.64} = 2.37$$

(Values above can all be corrected by dividing eff. factors by 1.07;
ratios stay constant. (RM 7/28/65)

Recheck Efficiency Factors for Storage Racks with Part #003

Vault Temp 66°F.

Position #	cts	Δt	c/m	c/s	d/s	eff. factor
26	13230 14964	20	1410 $M_s = 2.15$	23.5 3.72×10^5	3.98×10^5	6.31×10^{-5} (point) 5.90
1	15096 12486	20	1379	23.0		6.18×10^{-5} 5.78
2	18740 14777	20	1676	27.9		7.50×10^{-5} 7.01
39	9199 13291	20	1124	18.7		3.03×10^{-5} 4.70
40	10492 14098	20	1229	20.5		5.11×10^{-5} 5.15
25	12275 13280	20	1278	21.3		5.73×10^{-5} 5.36
3	13641 13902	20	1377	23.0		6.18×10^{-5} 5.78
5	12735 14490	20	1361	22.7		6.10×10^{-5} 5.70
6	15088 17533	20	1631	27.2		7.31×10^{-5} 6.83
7	11489 15402	20	1344	22.4		6.02×10^{-5} 5.63
8	13589 18503	20	1605	26.8		7.20×10^{-5} 6.73
26	12990 14909	20	1395	23.3		6.26×10^{-5} 5.85

Part is very much cooler to the touch than when removed from building this morning.

✓
7-12-65

Posn. #	Counts	Δt	e/m	e/sec	d/s 3.98×10^{-5}	eff factor
4	16846 16372	20	1661	27.7		7.45×10^{-5} 6.96
9	9947 15565	20	1276	21.3		5.73×10^{-5} 5.36
10	12107 18841	20	1547	25.8		6.94×10^{-5} 6.49
11	13091 11523	18	1367	22.8		6.13 5.73
12	17229 13715	20	1547	25.8		6.94 6.49
13	13838 14047	20	1394	23.2		6.24 5.83
14	15880 15569	20	1572	26.2		7.04 6.58
15	10534 11227	16	1360	22.7		6.10 5.70
16	14375 16245	20	1531	25.5		6.85 6.40
17	10358 12988	18	1297	21.6		5.81 5.43
18	10457 14067	16	1533	25.6		6.88 6.43
19	9946 14728	20	1234	20.6		5.54 5.18

Posn #	Counts	at	9m	c/sec	δt_s	eff factor
20	10619 15800	18	1468	24.5	$\frac{3.98}{3.72} \times 10^{-5}$	6.59×10^{-5} 6.16
21	30849 26297	11	1299	21.7		5.83 5.45
22	15532 13364	20	1445	24.1		6.48 6.06
23	12945 13274	20	1311 1415	21.9 23.6		5.89 6.34 5.50
24	667930 676212	940	1430	23.8		6.42 5.98
25	12385 13593 13514	22.5 20	1295	21.6		5.81 5.43
26	13429 14867	20	1415	23.6		6.34 5.93
27	12139 15893	22.5	1246	20.8		5.59 5.22
28	12333 15247	20	1379	23.0		6.18 5.78
29	10051 14909	21	1189	19.8		5.32 4.97
30	11206 4896 16404 15983	20	1359	22.7		6.10 5.70
31	13229 11157	20	1219	20.3		5.46 5.10

Posn. #	Counts	Δt	c/min	%/sec	δ/sec	Off. factor
32	13746 12265	20 min	1301	21.7	3.98×10^{-5}	5.83 5.45
33	11723 12564	20	1214	20.2		5.43 5.07
34	12063 13201	20	1313	21.9		5.89 5.50
35	11396 12259	20	1183	19.7		5.30 4.95
36	12233 13795	20	1301	21.7		5.83 5.45
37	10035 13030	20	1153	19.2		5.16 4.82
38	11658 14175	20	1287	2.15		5.78 5.40
39						
40	10629 14132					
7/13-14						
Plug Ball	4516	1000	6.95	MO. 116		
Shelf 26	5645		10.16	169		
B6	362 513	273	3.21		Off factor $\frac{11.6 \times 10^{-2}}{2.41 \times 10^{-3}} = 4.82 \times 10^{-5}$	
					Essentially same as on p 34 (Suspect spurious contributions to leg count in this case)	

All multiplications in this series must be revised
downward by dividing by 1.11

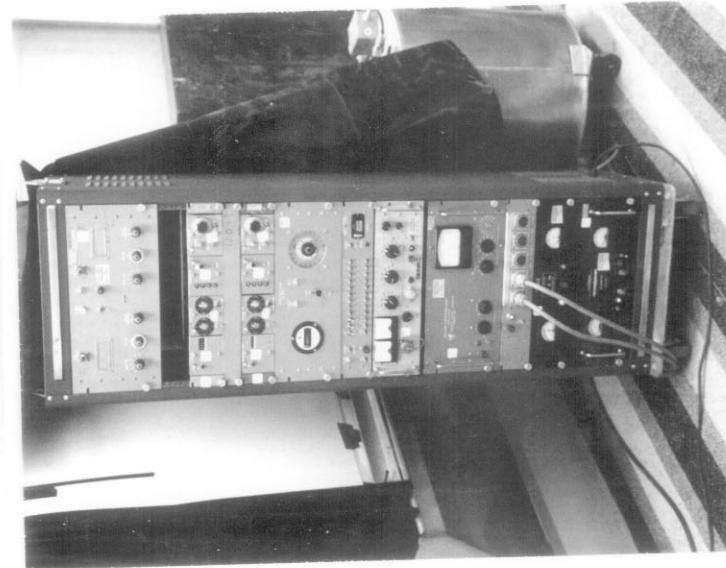
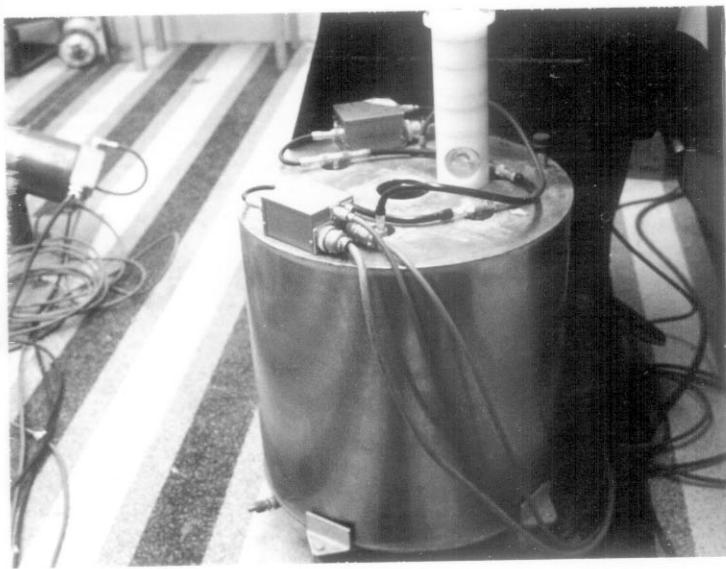
Part #	Posn	cts	Δt	%m	c/sec	$\Sigma d/s$	$\frac{d}{s}$	M ₂ Base Rate M
.003	5	13131 14999	20	1382	23.0	4.03 5.77 $\times 10^5$	1.85 $\times 10^5$	2.04 2.18 1.96
.008	7	12177 14847	10	2702	45.0	7.94 7.42 $\times 10^5$	3.64 $\times 10^5$	2.04 2.18 1.96
		B.R. 8				$1.79 \times 10^5 \text{n/s}$		
006	6	19617 24022	10	4364	72.7	12.0 11.2 $\times 10^5$	5.46 $\times 10^5$	2.06 2.19 1.97
		B.R. 6	$60.2 \times 3.029 = 1.82 \times 10^5 \text{n/s}$					

7/14/65

002 Temp in B.C. is 104°F after overnight in B Vault
at room temp 70°F . $\Delta T = 34^{\circ}\text{F}$

Repeat with 3, 6, and 8 as above

006	6	11889 14157	6	4341	essentially same as before			
002	8	13338 15682	5	5804	96.7	15.5 14.5 $\times 10^5$	7.30 $\times 10^5$	2.13 1.92
		B.R. = $60.8 \times 3.037 = 1.84 \times 10^5 \text{n/s}$						
004	15	13361 15583	4	7236	120.6	19.7 18.4 $\times 10^5$	9.09 $\times 10^5$	2.17 2.02 1.95
		B.R. = $59.4 \times 3.020 = 1.79 \times 10^5 \text{n/s}$						
009	17	11697 14050	3	8582	143.0	23.9 22.3 $\times 10^5$	10.9 $\times 10^5$	2.19 2.05 1.97
		B.R. = $60.3 \times 3.032 = 1.83 \times 10^5 \text{n/s}$						
005	16	14191 16409	3	10200	170.0	28.0 26.2 $\times 10^5$	12.7 $\times 10^5$	2.20 2.06 1.98
		B.R. = $59.2 \times 3.004 = 1.78 \times 10^5 \text{n/s}$						
001	18	14313 19014	3	11776	196.3	32.1 30.4 $\times 10^5$	14.5 $\times 10^5$	2.21 2.07 1.99
		B.R. = $60.5 \times 3.024 = 1.83 \times 10^5 \text{n/s}$						



<u>Part #</u>	<u>Posn</u>	<u>cts</u>	<u>Δt</u>	<u>U/m</u>	<u>c/sec</u>	<u>$\Sigma d/s$</u>	<u>Σ Base Rate</u>	<u>M</u> ³⁹
007	3	11917	2	13041	217.4	35.7 35.4×10^5	16.3×10^5	2.19 2.25 1.97

$$B.R. 59.2 \times 3.013 = 1.78 \times 10^5$$

Hence there is essentially no multiplication due to loading in stack.

7/15/65

After parts had been in A Vault overnight at room temp. of 68°F the indicated temperature of the instrumented part was 95°F : $\Delta T \approx 27^{\circ}\text{F}$

7/21/65 Critical Examination of ngs Situation

The Pu^{240} emission rate given in ANL 5800 p 715 is $1.02 \pm 0.02 \times 10^3 \text{n/g.s.}$. This was calculated from the partial fission half-life and the measured τ for spontaneous fission. Check this calculation:

Fission half life given for Pu^{240} is $1.22 \times 10^{11} \text{ yrs}$

Neutrons/fission (γ) is 2.23 ± 0.05 (this value is in good agreement with data from several sources)

$$\text{Then } \lambda_f = \frac{6.93 \times 10^{-1}}{1.22 \times 10^{11} \text{ yrs}} = 5.68 \times 10^{-12} \text{ yrs}^{-1}$$

$$\text{Convert to sec } \lambda_f = \frac{5.68 \times 10^{-12} \text{ yrs}^{-1}}{3.15 \times 10^7 \text{ sec/yr}} = 1.80 \times 10^{-19} \text{ sec}^{-1}$$

$$\text{Atoms/g} = \frac{6.02 \times 10^{23}}{2.40 \times 10^2} = 2.51 \times 10^{21}$$

$$\frac{dN}{dt} = \lambda_f N = (1.80 \times 10^{-19} \text{ sec}^{-1})(2.51 \times 10^{21} \text{ atoms/g}) = 4.52 \times 10^2 \text{ fiss./g.s.}$$

$$\frac{dp}{dt} \Rightarrow \frac{dN}{dt} = 4.52 \times 10^2 \times 2.23 = 1.01 \times 10^3 \text{n/g.s. which agrees with}$$

ANL 5800 number and checks their calculation error $\pm 2\%$ (± 0.02)

Using fission rate $4.61 \times 10^2 \text{ fiss./g.sec}$ [O. Chamberlain et al Phys Rev 156 (1954)] and

$$\bar{P}_{240}(\text{s.f.}) = 2.189 \pm 0.026 \quad [\text{Naphuis \& Diven Jmc Phys } \underline{48} \text{ 433-42}]$$

we get

$$\frac{dn}{dt} = (4.61 \times 10^2 \text{ fiss/sec}) (2.189 \text{ in/fiss}) = \underline{\underline{1.01 \times 10^3 \text{ m/g sec}}}$$

this is best value I can derive ($\sim \pm 1\%$)

Counter eff. for incline table Source P-11 1.42×10^7 n/sec ..

Pass ind.

	Counts / 2 min		c/m	
	Tub 1	Tub 2	T-1	T-2
full out	3972	23681	30570	11840
full in	15	14851	20233	15285

Cross check with Cf 252 fission source 1.04×10^6 n/sec
Source belonged to S. Block $\pm 4\%$.

	ctr		Ratio PuBe/Cf	
	10.00 min	10.00 min	10.97	11.14
full out	3973.5	10788	13022	1079
full in				1302

Rechecked with fission source and polyethylene block alongside the source

full out	3973.5	11393	13786	1139	1379
full in					

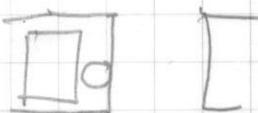
full out	3973.5	13025	3218	1303	322
full in					

Source P"

full out 39735

28335 / 2 min 9581 / 2 min 14168 c/min 4791 fm

Ratio PuBe/Cf 10.87 14.88



P"

full out 39735

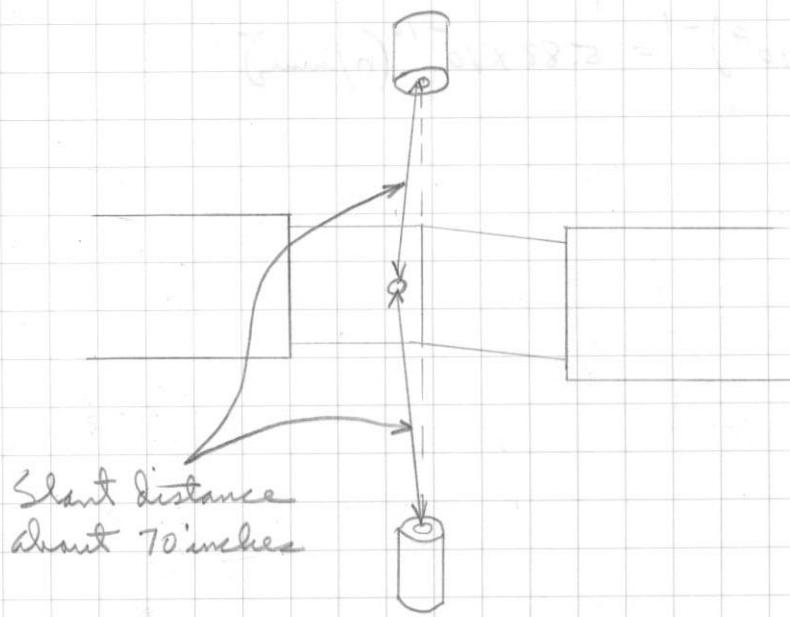
25857 32741 12979 fm 16371 fm

Ratio PuBe / CF 11.40 11.87

Ratio of emission rates as known is 14.2

Block will let us know calibration of fission source when done.

8/2/65 Considerable experimenting was required to obtain an arrangement of counters which provided a reasonably flat counter efficiency during the closure of the horizontal table. A suitable arrangement was as shown below:



A schedule of counter efficiency factors was measured for the travel of the table sections.

Horizontal Table Efficiency vs Position

Position, cm	Count Rate T-1 / 2 min	Efficiency		Count Rate T-2 / 2 min	Efficiency	
		Norm. to Pos. 0.00 = 1.00	T-1		Norm. to Pos. 0.00 = 1.00	T-2
0.00	12713	7.48 × 10 ⁻⁶	1.00	15374	9.04 × 10 ⁻⁶	1.00
5.00	12534	7.37	0.985	15334	9.02	0.997
10.00	12768	7.51	1.00	15265	8.98	0.993
15.00	12761	7.50	1.00	15455	9.09	1.02
20.00	13058	7.68	1.03	15564	9.15	1.01
25.00	13216	7.77	1.04	15709	9.24	1.02
30.00	13218	7.77	1.04	15700	9.23	1.02
40.00	13500	7.94	1.06	15758	9.27	1.03
50.00	13424	7.89	1.05	15935	9.37	1.04

(Vertical table was fully down)

To convert emission rate - source P-11 to counts / min.

$$1.20 \times 10^2 \text{ sec/min} \times 1.42 \times 10^7 \text{ m/sec} = 1.70 \times 10^9 \text{ m/min}$$

$$\text{Iscom. factor} = (1.70 \times 10^9)^{-1} = 5.88 \times 10^{-10} (\text{n/mm})^{-1}$$

Incline Table Efficiency vs Position

Norm. to Pos. 0.00 = 1.00

O

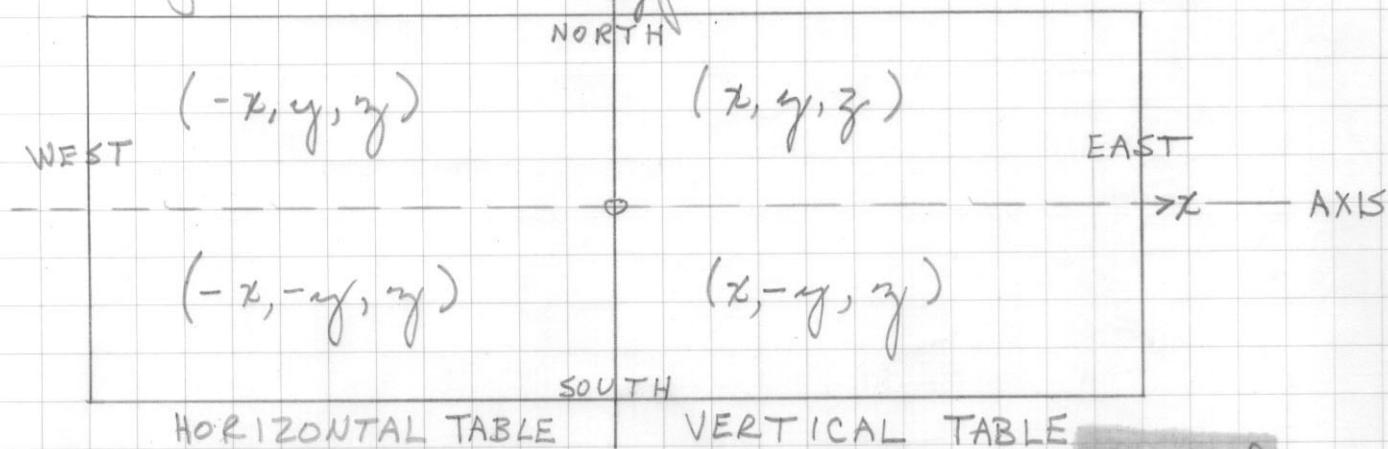
Position cm	Count Rate T-1 / 2 min	Efficiency T-1	Count Rate T-2 / 2 min	Efficiency T-2	Norm. to Pos. 0.00 = 1.00
39.73	15160	8.91×10^{-6}	1.19 17972	10.57×10^{-6}	1.17
35.00	15125	8.89	1.19 17687	10.40	1.15
30.00	14729	8.66	1.16 17544	10.32	1.14
25.00	14128	8.31	1.11 17198	10.11	1.12
20.00	14225	8.36	1.12 16834	9.90	1.09
15.00	14048	8.26	1.10 16529	9.72	1.07
10.00	13578	7.98	1.07 16021	9.42	1.04
5.00	13175	7.75	1.04 15702	9.23	1.02
0.14	12682	7.46	1.00 15386	9.05	1.00

(Horizontal table was fully back)

8/2/65

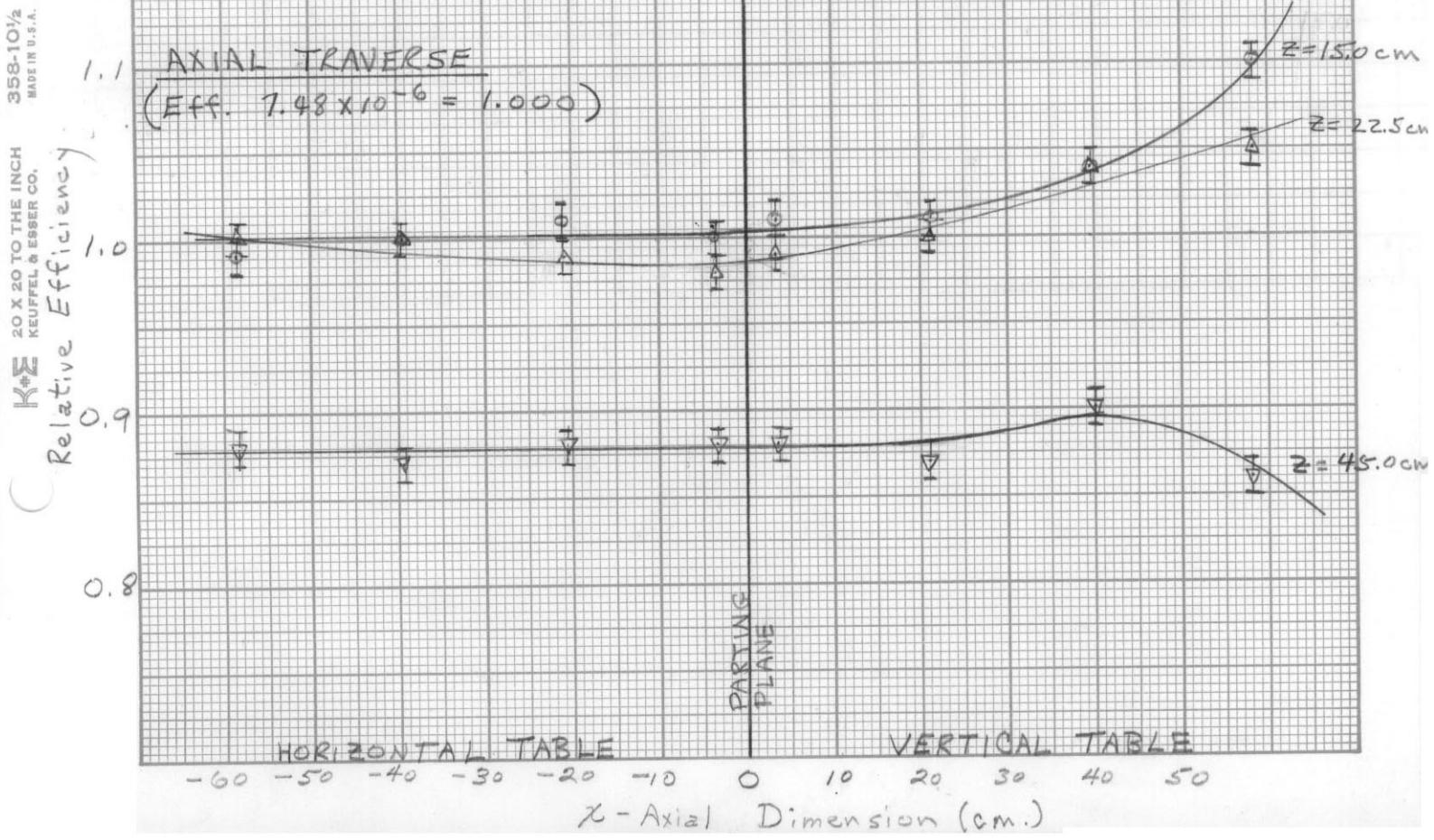
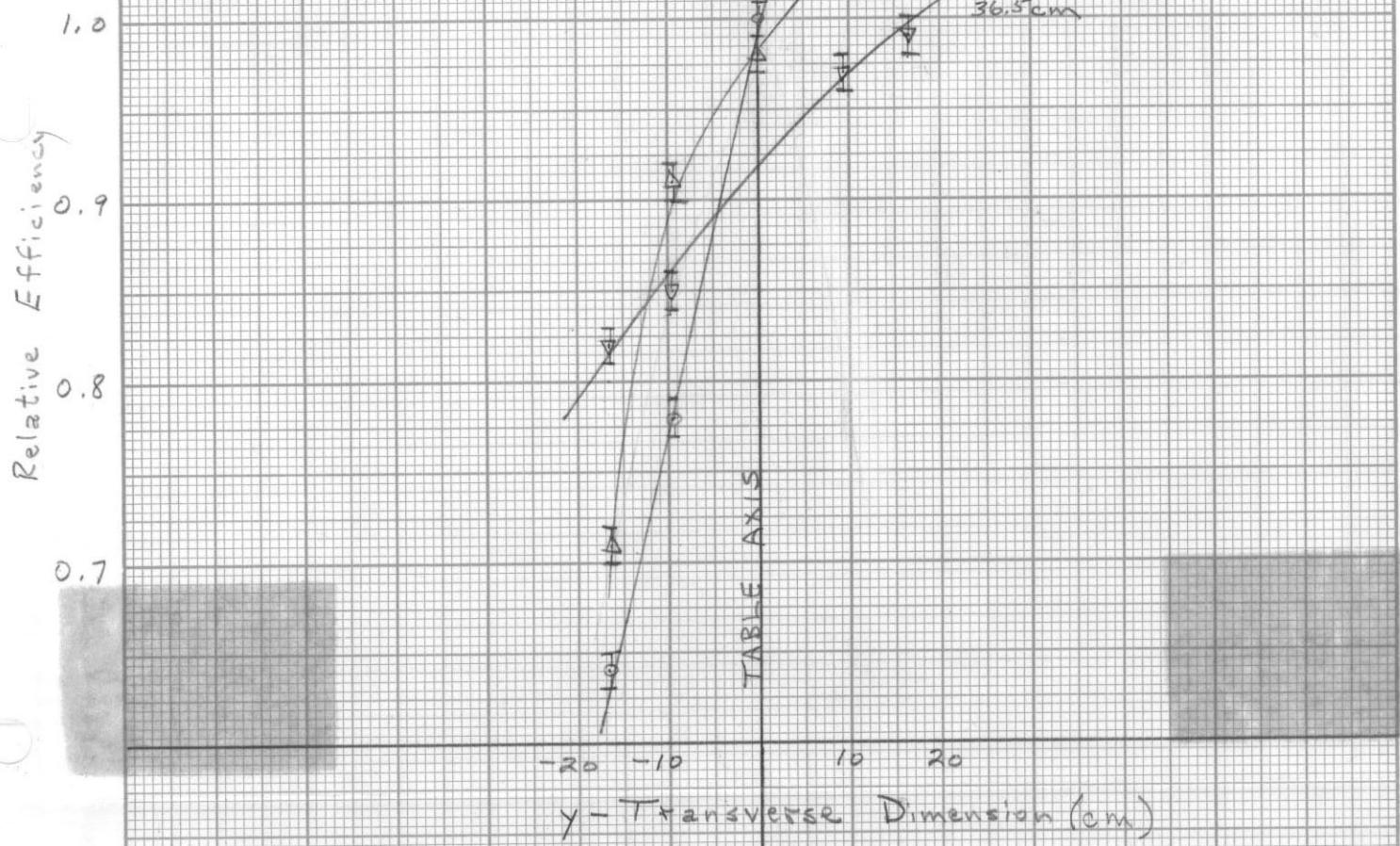
In order to describe the location of the source on the table, the following convention was adopted:

The table was divided into four quadrants with the origin at the center of the assembled halves.



The coordinates reported are the centers of the tube bases in centimeters. This orientation was selected because it coincided with the perspective view of the table through the TV monitor. For the z dimension the measurement given is from the table top to the base of the source or part. A minus coordinate will be the indicated position of the table indicated by the sign of z .

Counter 1 Transverse & Axial Variations in Counter Efficiency



A study was then made of the geometry down the axis of the table with both parts fully closed together.

Horizontal table : 0.00, Vertical table 0.14.

Note here the x and y positions of the source were varied.

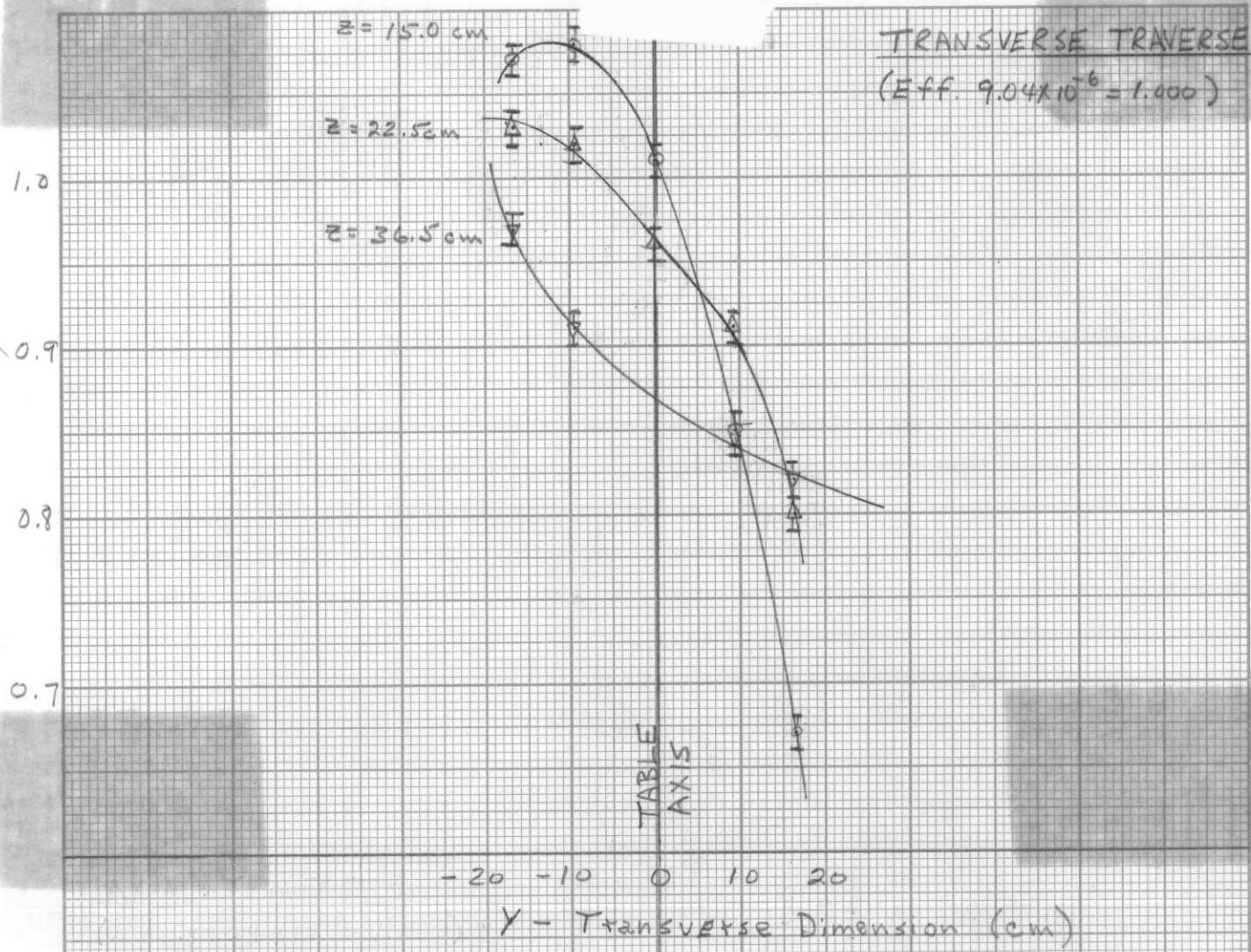
Source Position	Count Rate T-1 / min cm	Efficiency T_{-1}	Normalized to (-3.5,0,15) = 1.00	Count Rate T-2 / min	Efficiency T_{-2}	Normalized to (-3.5,0,15) = 1.00
-3.5,0,15-	12739	7.49×10^6	1.00	15546	9.14×10^6	1.01
-21.1,0,15-	12903	7.59	1.01	15896	9.35	1.03
-39.7,0,15-	12717	7.48	1.00	16475	9.69	1.07
-58.3,0,15-	12607	7.41	0.99	16387	9.64	1.07
-3.5,0,22.5	12542	7.37	0.98	14718	8.65	0.96
-21.1,0,22.5	12636	7.43	0.99	15394	9.05	0.99
same	12581	7.40	0.99	15399	9.05	0.99
-39.7,0,22.5	12694	7.46	1.00	15488	9.11	1.00
-58.3,0,22.5	12737	7.49	1.00	15133	8.90	0.97
-3.5,0,45	11212	6.59	0.88	12753	7.50	0.82
-21.1,0,45-	11058	6.50	0.88	12846	7.55	0.83
-39.7,0,45	11131	6.55	0.87	13236	7.78	0.85
-58.3,0,45	11197	6.58	0.88	13300	7.82	0.86
8/3/65-						
-3.5,0,15-	12854	7.56	1.01	15676	9.22	1.01
same	12654	7.44	0.99	15802	9.29	1.02
same	12712	7.47	1.00	15519	9.13	1.00
3.5,0,15	12843	7.55	1.01	15774	9.28	1.03
21.1,0,15-	12799	7.53	1.01	16534	9.72	1.08
39.7,0,15	13262	7.80	1.04	16682	9.81	1.09
58.3,0,15-	13969	8.21	1.10	16056	9.44	1.04
3.5,0,22.5	12562	7.39	0.99	15183	8.93	0.99
21.1,0,22.5	12777	7.51	1.00	15466	9.09	1.01
39.7,0,22.5	13207	7.77	1.04	15736	9.25	1.02
58.3,0,22.5-	13334	7.94	1.05	15774	9.28	1.03
3.5,0,45	11187	6.58	0.88	13195	7.76	0.85
21.1,0,45	11042	6.49	0.87	13345	7.85	0.86

Counter 2 - Transverse & Axial Variations in Counter Efficiency

Relative Efficiency

358-10^{1/2}
MADE IN U.S.A.

KEM 20 X 20 TO THE INCH
KEUFFEL & ESSER CO.



TRANSVERSE TRAVERSE

$$(\text{Eff. } 9.04 \times 10^{-6} = 1.000)$$

Relative Efficiency

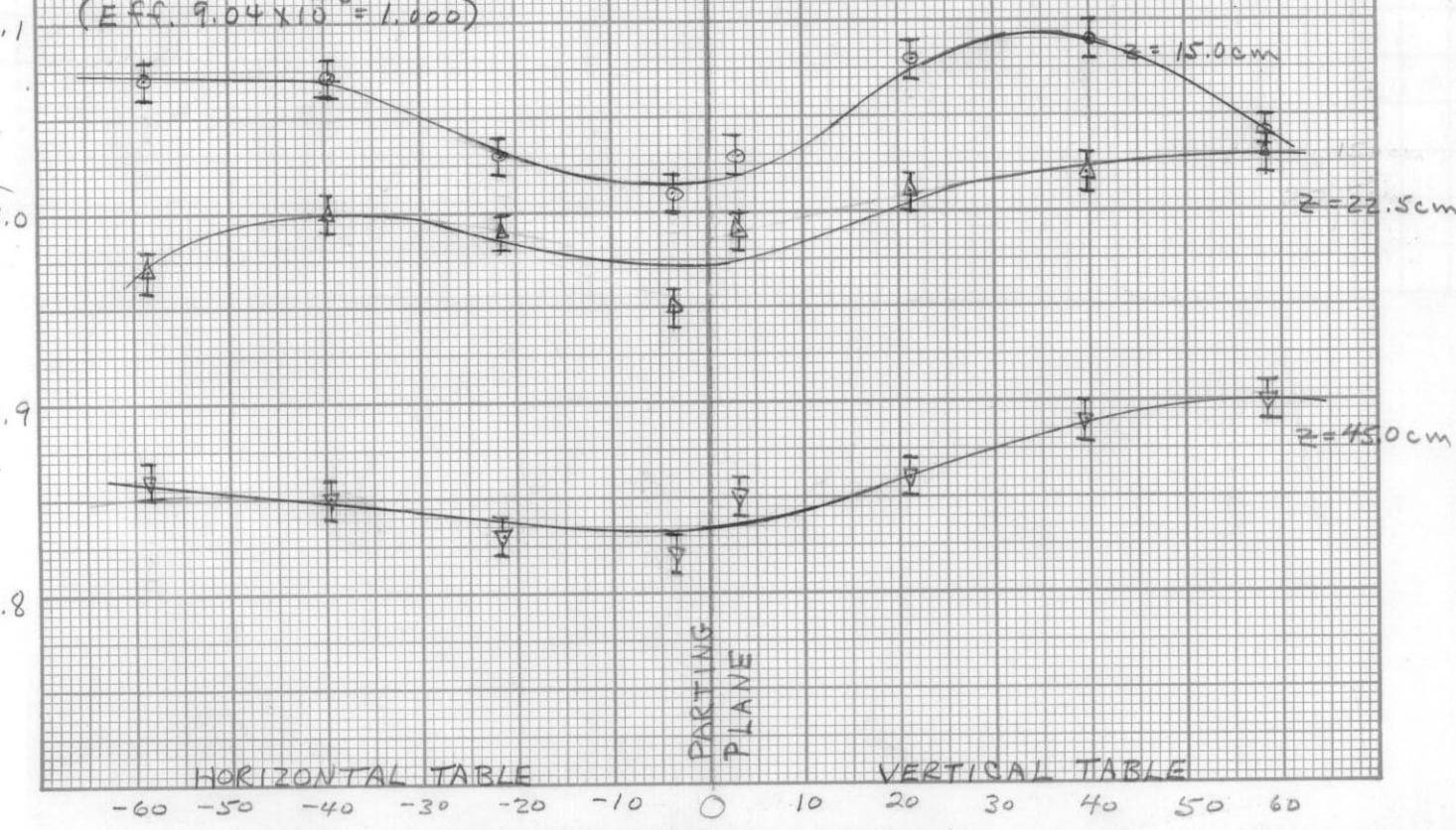
PARTING PLATE

VERTICAL TABLE

X - Axial Dimension (cm.)

AXIAL TRAVERSE

$$(\text{Eff. } 9.04 \times 10^{-6} = 1.000)$$



HORIZONTAL TABLE

-60 -50 -40 -30 -20 -10 0 10 20 30 40 50 60

Source Position	Count Rate T-1 / 2 min	Efficiency T-1	Normalized Count Rate to (-3.5, 0, 15) = 1.00	Count Rate T-2 / 2 min	Efficiency T-2	Normalized Count Rate to (-3.5, 0, 15) = 1.00
39.7, 0, 45	11480	6.75×10^6	0.90	13822	8.13×10^6	0.89
59.3, 0, 45	10920	6.42	0.86	13961	8.21	0.90
39.7, 0, 45	11520	6.77	0.90	13782	8.10	0.89

Following series evaluated effect of having empty tubes near source

○
×
○

-3.5, 0, 15	12261	7.21	0.96	14639	8.61	0.94
<i>Empty tubes removed</i>						
-3.5, 0, 15	12662	7.45	0.99	15332	9.02	0.99
same	12885	7.58	1.01	15693	9.23	1.01
<i>Single D-38 part placed in tubes beside one containing source</i>						
-3.5, 0, 15	12089	7.46	1.00	15248	8.97	0.98
same	12630	7.43	0.99	15103	8.88	0.97
<i>The fissions of U^{238} may have contributed to increase with D-38</i>						
-3.5, 0, 15	12154	7.14	0.95	14783	8.69	0.95
same	11943	7.02	0.94	14945	8.79	0.96

Tentative conclusions from above:

1. Presence of vertical table does not seem to alter the counter efficiency of the source on the horizontal table, but not vice versa.
2. The counting efficiency is essentially constant for ^{same} source elevations to $\approx \pm 20$ km.
3. A high degree of symmetry is not achieved through the plane of separation.

8/3/65

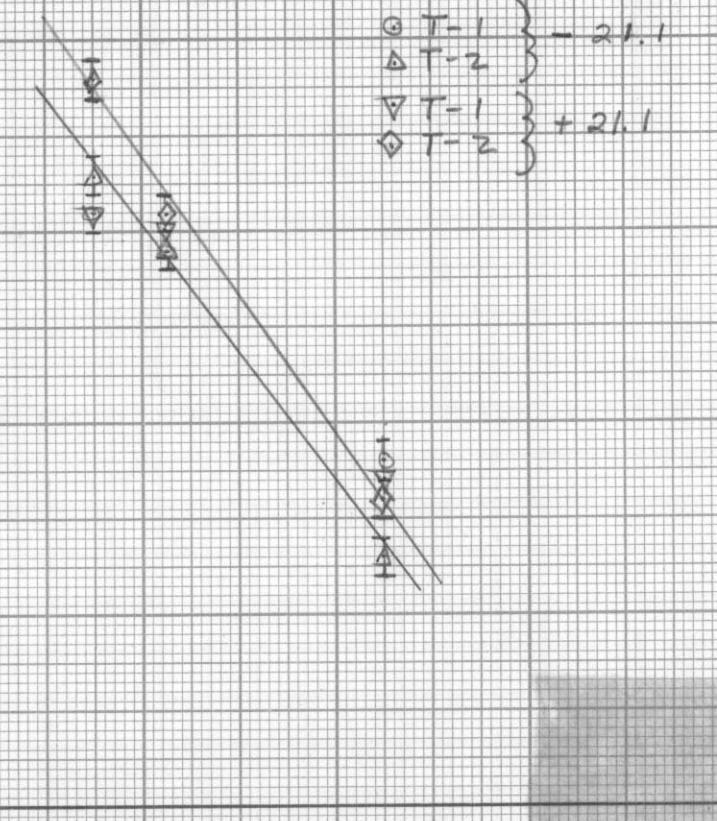
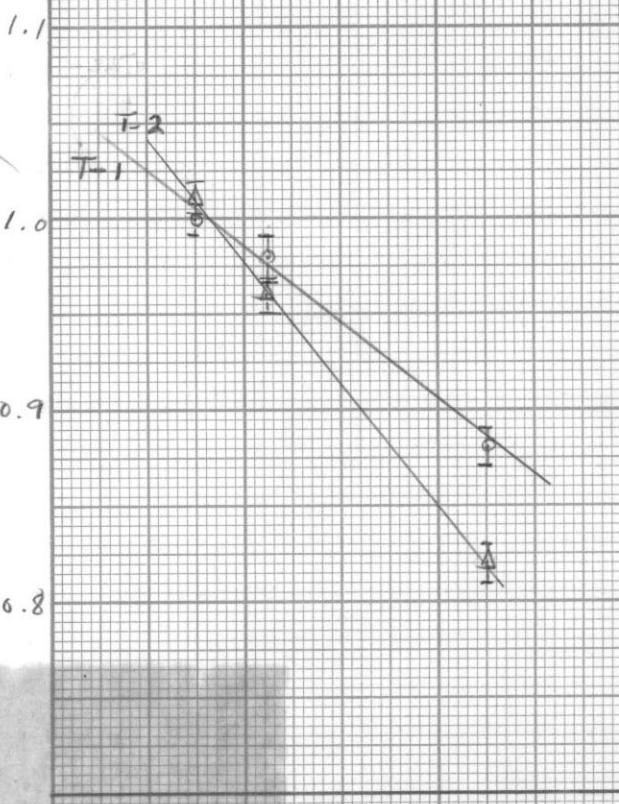
Following series evaluated effects of having source off the axis:

-3.5, 9.3, 15	13954	8.20	1.09	13032	7.66	0.85
-3.5, -9.3, 15	9925	5.84	0.78	16622	9.77	1.08
-3.5, 16.5, 15	13559	7.97	1.06	10378	6.10	0.67
-3.5, -16.5, 15	12216 / 3 min (8144)	4.79	0.64	24781 / 3 min (16521)	9.71	1.07
-3.5, -16.5, 22.5	13568 / 3 min (9046)	5.32	0.71	23736 / 3 min (15825)	9.31	1.03
-3.5, -16.5, 36.5	10450	6.14	0.82	14944	8.79	0.97
-3.5, 16.5, 36.5	12693	7.46	0.99	12596	7.41	0.82

Vertical Traverse $(-3.5, 0, z)$

Vertical Traverses $(\pm 21.1, 0, z)$

Relative Efficiency

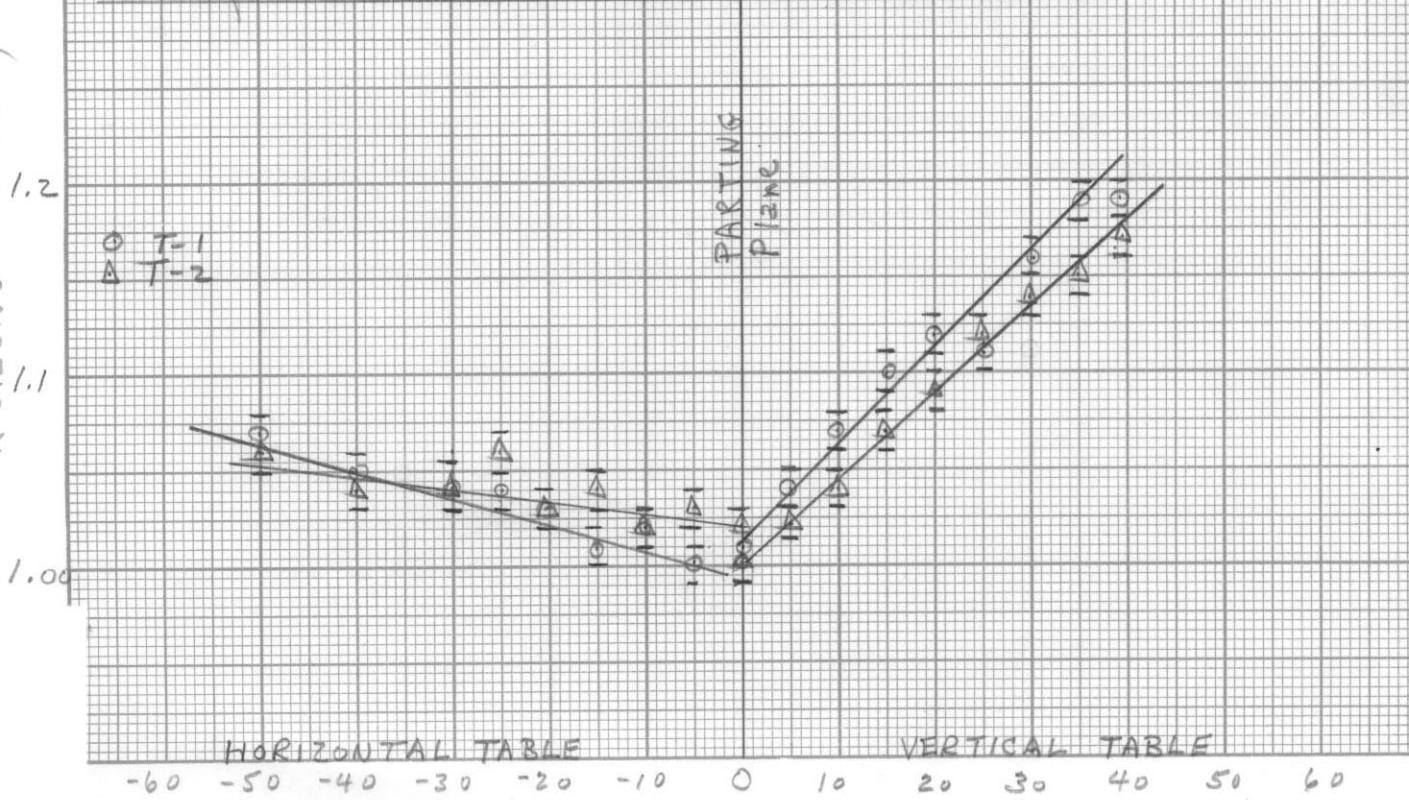


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Counter Efficiency Variation with Motion of Tables
in Sequence ① Vertical Table ② Horizontal Table

Relative Efficiency



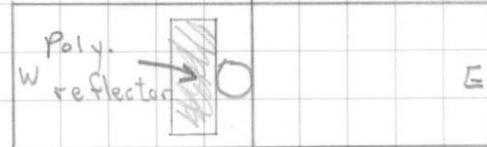
x - Axial dimension from full closure (cm)

Source Position cm -	Count Rate T-1 / 2 min	Efficiency T-1	Normalized to (-3.5, 0, 15) = 1.00	Count Rate T-2 / 2 min	Efficiency T-2	Normalized to (-3.5, 0, 15) = 1.00
-3.5, 16.5, 22.5	13712	8.06×10^{-6}	1.08	12274	7.22×10^{-6}	0.80
-3.5, 9.3, 22.5	13296	7.82	1.04	13938	8.20	0.91
-3.5, 9.3, 36.5	12404	7.29	0.97	12909	7.59	0.84
-3.5, -9.3, 36.5	10859	6.39	0.85	13953	8.20	0.91
-3.5, -9.3, 22.5	11528	6.78	0.91	15650	9.20	1.02

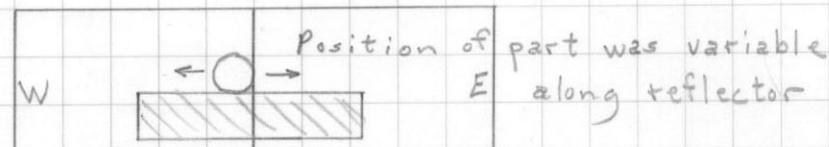
Following series is for determination of efficiencies for configurations to be used in Assembly Procedure 4:



-3.5, 0, 15	12197	7.17	0.96	13443	9.08	1.00
same	12175	7.16	0.96	15279	7.16	0.79
-3.5, 0, 22.5	12047	7.08	0.95	14235	8.37	0.93
-3.5, 0, 36.5	11167	6.57	0.88	13006	7.65	0.85



-3.5, 0, 36.5	11521	6.77	0.90	13495	7.94	0.88
same	11725	6.99	0.92	13264	7.80	0.86
-3.5, 0, 15	12995	7.64	1.02	15709	9.24	1.02
-3.5, 0, 22.5	12651	7.44	0.99	14733	8.66	0.96



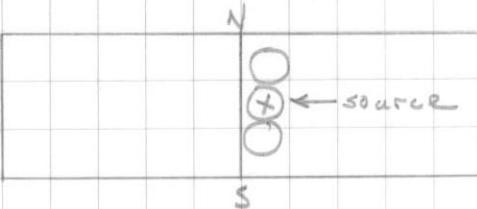
-3.5, 9.3, 22.5	17005	10.00	1.34	4851	2.85	0.315
same	16894	9.93	1.33	4801	2.82	0.312
same	17187	10.11	1.35	4827	2.84	0.314
same	17324	10.19	1.36	4813	2.83	0.313
same	17156	10.09	1.35	4839	2.85	0.315
-3.5, 9.3, 25.75	16924	9.95	1.33	4816	2.83	0.313
-3.5, 9.3, 36.5	15414	9.06	1.21	4530	2.66	0.294
-3.5, 9.3, 15	17800	10.47	1.40	5404	3.18	0.352
-11.0, 9.3, 15	17469	10.27	1.37	5433	3.19	0.353

Position cm	Count Rate T-1 / 2 min	Efficiency T-1	Normalized Count Rate to (-3.5, 0, 15)	Efficiency T-2 / 2 min	T-2	Normalized to (-3.5, 0, 15) = 1.00
-18.0, 9.3, 15	17023	10.0×10^6	1.34	5471	3.22×10^6	0.356
18.0, 9.3, 15	18026	10.60	1.42	5660	3.33	0.368
11.0, 9.3, 15	17896	10.52	1.40	5348	3.14	0.347
3.5, 9.3, 15	17873	10.51	1.40	5424	3.19	0.353
3.5, 9.3, 25.75	16855	9.91	1.32	4679	2.75	0.304
3.5, 9.3, 36.5	15350	9.03	1.21	4708	2.77	0.306

Following series has same arrangement as above but reflector is absent:

3.5, 9.3, 36.5	12466	7.33	0.98	12958	7.62	0.84
-11.0, 9.3, 15	13871	8.16	1.09	14142	8.32	0.92
-18.0, 9.3, 15	13589	7.99	1.07	14571	8.57	0.95
11.0, 9.3, 15	13808	8.12	1.08	14969	8.80	0.97

Following series was to investigate the effect of the presence of D-38 parts positioned between counters and source:



Both lateral tubes empty

-3.5, 0, 15	11515	6.79	0.90	14149	8.32	0.92
D-38 in south tube						
-3.5, 0, 15	12386	7.28	0.97	14199	8.35	0.92
D-38 in both tubes						
-3.5, 0, 15	12605	7.41	0.99	15408	9.06	1.00
D-38 in north tube						
-3.5, 0, 15	11878	6.98	0.93	14476	8.51	0.94
same	12284	7.22	0.96	14857	8.74	0.97

Following series was to check counter efficiency for motion of horizontal table, vertical table up:

-3.5, 0, 15, 0	12814	7.53	1.01	15618	9.18	1.02
5	12787	7.52	1.00	15784	9.28	1.03
10	12964	7.62	1.02	15674	9.22	1.02
15	12922	7.60	1.01	15933	9.37	1.04
20	13133	7.72	1.03	15873	9.33	1.03
25	13307	7.82	1.04	16038	9.59	1.06
30	13279	7.81	1.04	15921	9.36	1.04
40	13437	7.90	1.05	16061	9.44	1.04
50	13759	8.09	1.08	16225	9.54	1.06

Obviously, for neutron counting purposes, the position of the vertical stable interacts with the counters observing the variations in count-rate while the horizontal table moves; therefore the preceding values will apply in practical situations rather than those on page 41.

8/5/65

Results of billet self-multiplication on assembly table.

Billet Position	Count/50 min	n/sec	M_s	Count/50 min	n/sec	M_s
	$T-1$			$T-2$		
001 -3.5, 0, 15, 0, 0	10873	4.83×10^5	2.38	13651	4.98×10^5	2.45
002 -3.5, 0, 15, 0, 0	11212	4.98×10^5	2.43	14169	5.17×10^5	2.53
004 -3.5, 0, 15, 0, 0	10935	4.87×10^5	2.45	13388	4.88×10^5	2.45
005 -3.5, 0, 15, 0, 0	10599	4.72×10^5	2.39	13233	4.83×10^5	2.45
006 -3.5, 0, 15, 0, 0	11110	4.95×10^5	2.45	13754	5.02×10^5	2.48
007 -3.5, 0, 15, 0, 0	10682	4.75×10^5	2.40	13339	4.87×10^5	2.46
8/6/65						
008 -3.5, 0, 15, 0, 0	11290	5.02×10^5	2.49	13938	5.08×10^5	2.53
009 -3.5, 0, 15, 0, 0	11029	4.91×10^5	2.42	13074	5.00×10^5	2.47

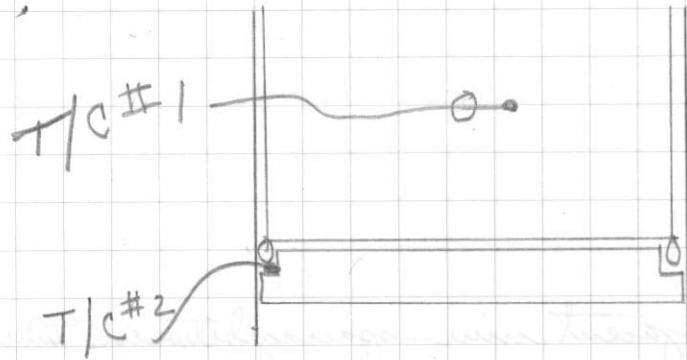
8/6/65

Thermocouples #1 and 2 were calibrated to $32^\circ F$ in an ice water bath and then checked at room temperature ($73^\circ F$) using a mercury thermometer as a secondary standard. They were in good correlation as indicated on the thermocouple strip chart recorder.

8/9/65 Study of Billet Temperature in Support Tube

48

The following series of measurements was performed to determine the adequacy of the heat transfer properties of the billet support tubes. Part number 008 was used for this purpose. It was placed in the tube ~6 in. above the tube top. The tube was open above it. The T/C's were located as shown in the sketch.



Initially indicated temperatures were 73°F at assembly machine.

Tire	T/C 1	T/C 2
0850	93.5	94
1100	91	92
1300	90	91

This shows gradual cooling over about 2 hrs after taking out of box. Then essentially constant. At about 1320 we decided to see how much additional help in cooling would be provided by an electric fan.

1400 81 82
After this level was reached, the temperature essentially stabilized,

heat transfer

and turbulent flows

N heat tubes are adjacent min. spacing between tubes
is 0.05 cm .

Outer can surface is $\sim 0.30\text{ cm}$ within outer tube surface.

So min. distance laterally can to can is $\sim 0.65\text{ cm}$

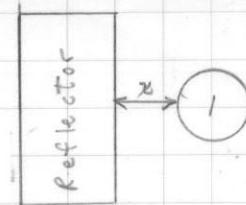
with can wall thickness of 0.010 in (0.025 cm)

we then have min. spacing part-to-part of
 $\sim 0.70 \pm 0.02\text{ cm}$.

(See page 67 and 20 for more correct
values of these dimensions)

8/10/65

First Assembly (A-1)



Part 001, position $3.5, 0, 15$; Base rate = 2.030×10^5

T/C's as shown p 48 #1, $92^\circ F$; #2, $88^\circ F$; Room temp $72^\circ F$

Table Pos.	T-1	Eff	n/sec	M	T-2	Eff	n/sec	M
cm.	s/s/50 min	Factor			s/s/50 min	Factor		
vert.								
39.73	13005	8.91×10^{-6}	4.86×10^5	2.39	17063	10.57×10^{-6}	5.37×10^5	2.65
0.14	11058	7.46	4.95	2.44	13814	9.05	5.08	2.50
Horiz.								
05.9								
9.555	11149	7.64	4.87	2.40	13970	9.24	5.04	2.48
0.000	8396/38	7.64	4.82	2.37	10391/38	9.24	4.94	2.44

8/11/65

2d Assembly (A-2)



x = distance between parts

Parts 001, position $3.5, 9.3, 15$; Base rate = 2.030×10^5

002, position - $3.5, 9.3, 15$; Base rate = 2.047×10^5

T/C's still on 001, #1 = $86^\circ F$; #2 = $86^\circ F$, Room temp $71^\circ F$

-39.73	$15560/25(001)10.60 \times 10^{-6}$				$7219/25(001)3.33 \times 10^{-6}$			
65.9 H		(002) 10.01				(002) 3.22		
	Ave. 10.3		10.07	2.47		Ave. 3.27	14.70	3.61
-0.14 V	$14509/25(001)10.51$				$6449/25(001)3.19$			
65.9 H		(002) 10.01				(002) 3.22		
	Ave. 10.25		9.43	2.31		Ave. 3.20	13.44	3.30

8/12/65

-0.14 V	$15512/25(001)10.51$				$5027/25(001)3.19$			
9.569		(002) 10.27				(002) 3.19		
	Ave. 10.39		9.95	2.44		Ave. 3.19	10.5	2.58

-0.14 V	$20048/25(001)10.51$				$5112/25(001)3.19$			
0.00		(002) 10.47				(002) 3.18		
	Ave. 10.49		12.74	3.12		Ave. 3.19	10.68	2.62

3d Assembly (A-3)

4 2 1

--	--	--

$$\begin{array}{lll}
 \text{Part} & \text{position} & \text{base rate} = \\
 001, & 3.5, 9.3, 15, & 2.030 \times 10^5 \\
 002, & -3.5, 9.3, 15, & 2.047 \times 10^5 \\
 004, & -11, 9.3, 15, & 1.990 \times 10^5 \\
 & & \text{Total} \quad 6.067 \times 10^5
 \end{array}$$

T/C son #1 as before #1 86°; #2, 87°; Room Temp. 71°F

Table Pos cm	T-1 cts/15min	Eff Factor	n/sec $\times 10^{-5}$	M	T-2 cts/15min	Eff Factor	n/sec $\times 10^{-5}$	M
39.71	16085	(001) 10.60	$\times 10^{-6}$		6473	(001) 3.33	$\times 10^{-6}$	
65.91		(002) 10.01	$\times 10^{-6}$			(002) 3.22	$\times 10^{-6}$	
		(004) 10.01	$\times 10^{-6}$			(004) 3.22	$\times 10^{-4}$	
	Ave. 10.21	17.5	2.89		Ave. 3.26	22.1	3.65	
0.14V	15463	(001) 10.51			5977	(001) 3.19		
65.91		(002) 10.01				(002) 3.22		
		(004) 10.01				(004) 3.22		
	Ave. 10.14	16.94	2.80		Ave. 3.21	20.7	3.42	
0.14V	16171	(001) 10.51			4931	(001) 3.19		
9.5691		(002) 10.27				(002) 3.19		
		(004) 10.01				(004) 3.22		
	Ave. 10.26	17.50	2.89		Ave. 3.20	17.12	2.83	
0.14V	20122	(001) 10.51			4745	(001) 3.19		
0.00W		(002) 10.47				(002) 3.18		
		(004) 10.27				(004) 3.19		
	Ave. 10.42	21.46	3.55		Ave. 3.19	16.52	2.73	

Parts 001, position 3.5, 9.3, 15, base rate = 2.030×10^5

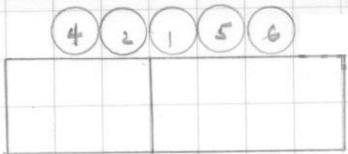
002,	- 3.5, 9.3, 15,	2.047
004,	- 11, 9.3, 15	1.990
005,	11, 9.3, 15	1.974
	Total	8.041×10^{-5}

$$\text{Total} \quad 8.041 \times 10^5$$

T/C's on 001 as before # 1 = 94°F; # 2 = 86°F; Room temp

Table No.	T-1 cm -	Eff to/10 min	n/sec $\times 10^{-5}$	M	T-2 to/10 min	Eff to/10 min	n/sec $\times 10^{-5}$	M
39.7V	23277/15	(001) 10.60×10^{-6} (002) 10.01×10^{-6} (004) 10.01×10^{-6} (005) 10.60×10^{-6}			8528/15	(001) 3.33×10^{-6} (002) 3.22×10^{-6} (004) 3.22×10^{-6} (005) 3.33×10^{-6}		
65.9H	-	Ave. 10.3	25.11	3.12		Ave. 3.27	28.99	3.61
0.14V	14646	(001) 10.51×10^{-4} (002) 10.01 (004) 10.01 (005) 10.51			5085	(001) 3.19×10^{-4} (002) 3.22 (004) 3.22 (005) 3.19		
65.9H	-	Ave. 10.25	23.81	2.96		Ave. 3.20	26.50	3.30
0.14V	15577	(001) 10.51×10^{-6} (002) 10.01 (004) 10.27 (005) 10.52			4454	(001) 3.19×10^{-6} (002) 3.22 (004) 3.19 (005) 3.14		
9.56H	-	Ave. 10.33	25.13	3.13		Ave. 3.19	23.26	2.89
0.14V	18987	(001) 10.51×10^{-6} (002) 10.47 (004) 10.27 (005) 10.52			4455	(001) 3.19×10^{-6} (002) 3.18 (004) 3.19 (005) 3.14		
6.02H	-	Ave. 10.44	30.32	3.77		Ave. 3.18	23.36	2.90

5th Assembly (A-5)



Paths 001 position 3.8, 9, 3, 15, basetake = 2.030×10^5

202	-3.5, 9.3, 15	2.047
004	-11, 9.3, 15	1.990
005	11, 9.3, 15	1.974
006	18, 9.3, 15	2.023

$$\text{Total } 10.064 \times 10^5 \text{ n}^{\text{s}}/\text{sec}$$

T(c's on #00) as per: #1 = 94°, #2 = 90°F, Reson temp. 71°F

Ave. 10.37 33.83 3.36 Ave 3.21 30.03 2.99
8/13 T/C's #1 97°F, #2 92°F Room temp 71°F

0.14 V						
0.00 H	2495-9	1	10.51	5774	1	3.19
	2	10.47		2	3.18	
	4	10.27		4	3.19	
	5	10.52		5	3.14	
	6	10.60		6	3.33	
Ave.	10.47	39.57	3.93	Ave.	3.21	29.97
						2.98

6th Assembly (A - G)

(2) $\left\{ \begin{matrix} 4 \\ 1 \end{matrix} \right.$

Parts 001, position 3.5, 9.3, 15	base rate	2.030×10^5
002	- 3.5, 9.3, 15	2.047
004	3.5, 9.3, 19.6	1.990

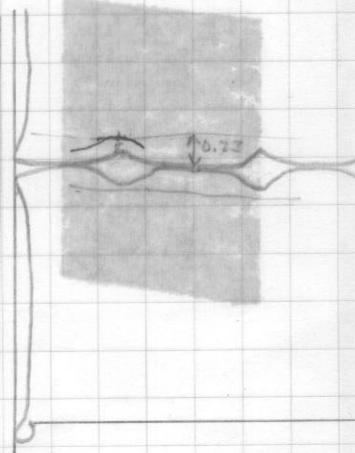
Total 6.067×10^5 n/sec

T/C's on 001 with 004 above it: #1 - 102°F, #2 - 93°F, Room temp. 71°F

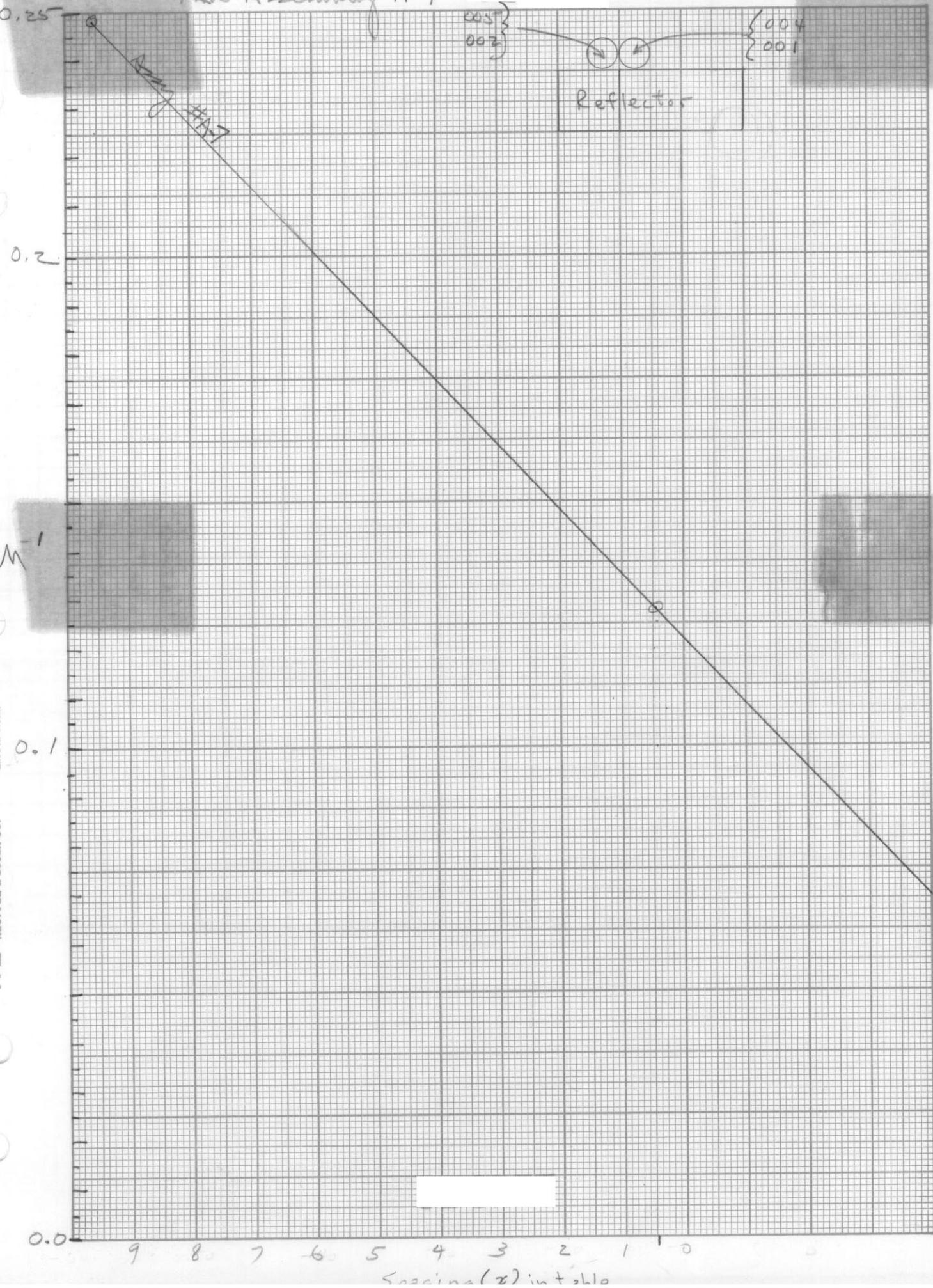
Table Pos. cm	T-1 cts/15min	Eff Factor	n/sec $\times 10^{-5}$	M	T-2 cts/15min	Eff Factor	n/sec $\times 10^{-5}$	M
0.141	175.85	(1) 10.51 $\times 10^6$ (2) 10.01 (4) 10.51			6771	(1) 3.19 $\times 10^6$ (2) 3.22 (4) 3.19		
9.551	19461	(1) 10.51 (2) 10.27 (4) 10.51			6064	(1) 3.19 (2) 3.19 (4) 3.19		
		Ave 10.34	18.89	3.11			Ave 3.20	23.50 3.87
0.141	T/C's #1 - 103°F, #2 - 94°F							
9.551	19461	(1) 10.51 (2) 10.27 (4) 10.51			6064	(1) 3.19 (2) 3.19 (4) 3.19		
		Ave 10.43	20.59	3.39			Ave 3.19	21.13 3.48
		T/C's #1 - 104°F, #2 - 94°F						
0.141	27172	(1) 10.51			6428	(1) 3.19		
0.001		(2) 10.47				(2) 3.18		
		(4) 10.51				(4) 3.19		
		Ave 10.50	28.75	4.74			Ave 3.19	22.38 3.69

The cans loaded in tandem were arranged as shown - bottom to bottom. This caused no. 001 (on the bottom) to heat up more than before

Part-to-part separation is 0.46 cm
(see B. Elliott's notes)



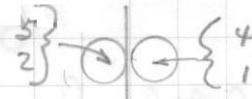
~~The~~ Assembly A-7



Part	001	, position	$3.5, 9.3, 15$	base rate	2.030×10^5
	002		$-3.5, 9.3, 15$		2.047
	004		$3.5, 9.3, 19.6$		1.990
	005		$-3.5, 9.3, 19.6$		1.974
				Total	8.041×10^5 sec

T/C's still on part 001, readings as below-

8th Assembly (A-8)
(Same as A-7 but reflector absent)

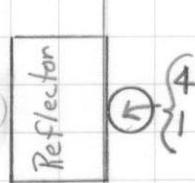


Parts 001, 002, 004, 005 positions (same as 7th)
Base rate 8.041×10^5 n/sec

T/C's still on part 001, #1 - 100°F, #2 - 95°F Room - 71°F

Table Pos cm	T-1 cts/15min	Eff. Factor	n/sec $\times 10^{-5}$	M	T-2 cts/15min	Eff. Factor	n/sec $\times 10^{-5}$	M
0.14 V		(1) 9.20 $\times 10^{-6}$				(1) 7.66 $\times 10^{-6}$		
0.00 H		(2) 8.20				(2) 7.66		
		(3) 7.82				(3) 8.20		
		(4) 7.82				(4) 8.20		
		(5) 7.82				(5) 8.20		
Avg. 8.01		47.71	5.93			Avg. 7.93	50.18	6.24

9th Assembly (A-9)



Parts 001, position 3.5, 0.0, 15.0, base rate 2.030×10^5 n/sec

004, 3.5, 0.0, 19.6 $\frac{1.990 \times 10^5}{4.020 \times 10^5}$

T/C's on 1 and 4 : #1 - 101°F, #2 - 97°F (May not have been in good contact)
Room Temp. 71°F

Table Pos. cm	T-1 cts/15min	Eff. Factor	n/sec $\times 10^{-5}$	M	T-2 cts/15min	Eff. Factor	n/sec $\times 10^{-5}$	M
0.14 V	10349	(1) 7.64 $\times 10^{-6}$			12099	(1) 9.24 $\times 10^{-6}$		
0.00 H		(4) 7.12				(4) 8.67		
		Avg. 7.38	15.58	3.88		Avg. 8.95	15.02	3.74

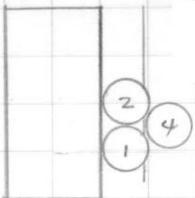
Used sound tube bases.
Gave surface to surface contact
for tubes - min. can separation
 $0.60 \text{ cm} \pm 0.02$

Use same geometry factor for entire group (This is for joint centered at 15 cm elevation inside plastic block.)

8/17/65

10th Assembly (A-10)

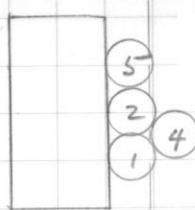
56



Part	001	, position -2.5,-7,15, base rate	2.030×10^5
	002	, -2.5, 0, 15	2.047
	004	, 3.5,-35,15	1.990

T/C #1 on part 001, T/C #2 on part 004; Total 6.067×10^5 m/sec

11 Assembly (A-1)



Part 001, position -2.5, -7, 15, base rate 2.030

002	-2.5, 0, 15	2.047
004	3.5, -3.5, 15	1.990
005	-2.5, 7, 15	1.974

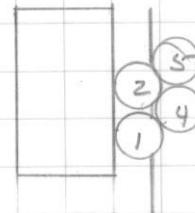
Total 8.041×10^5 n/sec

T/C's same as for 10th assembly

Table Pos. Cm	T-1 cts/10mm	Eff Factor	n/sec $\times 10^{-5}$	M	T-2 cts/10mm	Eff Factor	n/sec $\times 10^{-5}$	M
0.14V 65.9 H	11892	Ave. 7.64×10^{-6}	25.94	3.23	14173	9.24×10^{-6}	25.56	3.18
		T/C's #1-83°F, #2-83°F,				Room 71°F		
0.14V 9.55H	11129	7.64	24.26	3.02	13572	9.24	24.48	3.04
0.14V 0.00H	13572	7.64	29.61	3.68	17427	9.24	31.43	3.91
		T/C's #1-83; #2-83;				Room 71°F		

12th Assembly (A-12)

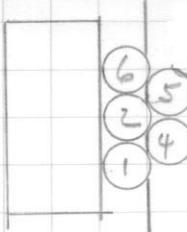
Same as 11 except part 005-
at 3.5, 3.5, 15



0.14V 65.9 H	10417	7.64	22.72	2.83	13143	9.24	23.71	2.95
0.14V 9.55H	10674	7.64	23.29	3.04	13649	9.24	24.62	2.66
0.14V 0.00H	15647	7.64	34.14	4.25	20309	9.24	36.63	4.56

T/C's #1-85°F; #2-85°F; Room 71°F

13th Assembly (A-13)



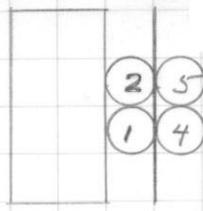
Part 001, position -2.5, -7, 15	base rate	2.030×10^5
002	-2.5, 0, 15	2.047
004	3.5, -3.5, 15	1.990
005	3.5, 3.5, 15	1.974
006	-2.5, 7, 15	2.023
		$10.064 \times 10^5 \text{ m/sec}$

T/C's on parts #001, 004

Table Pos cm	T-1 cts/7min	Eff Factor	n/sec $\times 10^{-5}$	M	T-2 cts/7min	Eff Factor	n/sec $\times 10^{-5}$	M
39.7 V	10491	Ave 7.64×10^6	33.31	3.31	12684	Ave 9.24×10^6	32.68	3.25
65.9 H		T/C's #1-84°F, #2-84°F, Room						71°F
0.14 V	10133	7.64	31.58	3.14	12350	9.24	31.77	3.16
65.9 H		T/C's #1-84°F, #2-84°F, Room						71°F
0.14 V	10250	7.64	31.94	3.17	12404	9.24	31.96	3.18
9.55 H		T/C's #1-83°F, #2-84°F, Room						71°F
0.14 V	17120	7.64	53.35	5.30	20815	9.24	53.64	5.33
0.00 H		T/C's #1-83°F, #2-84°F, Room						71°F

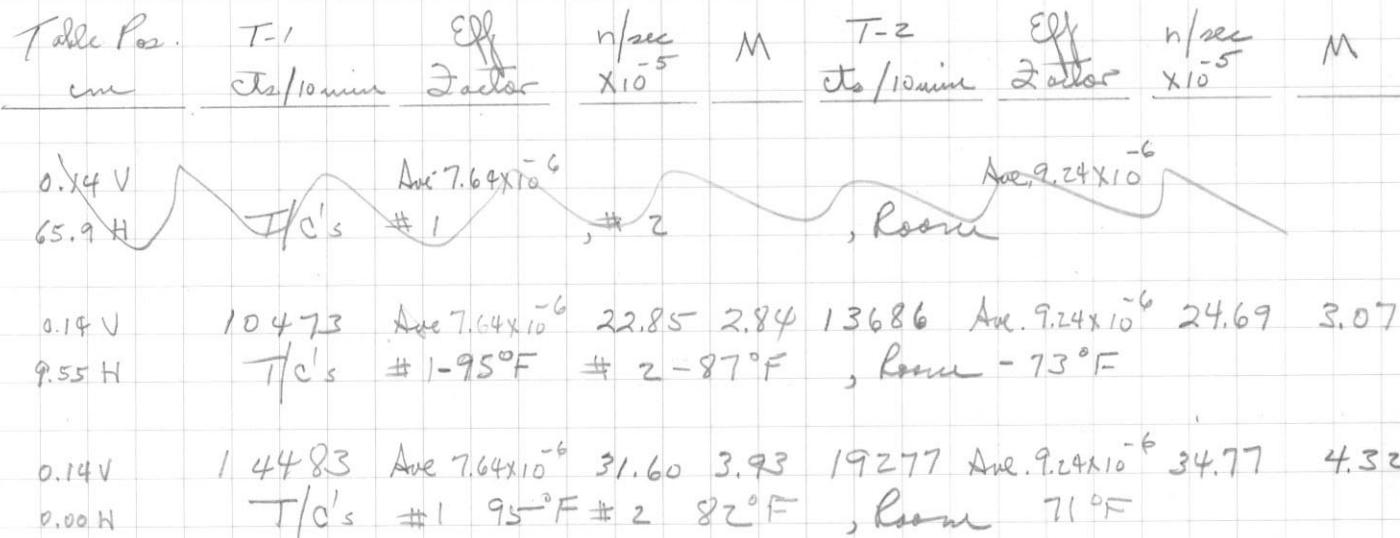
8/18/65
14 th Assembly (A-14)

59



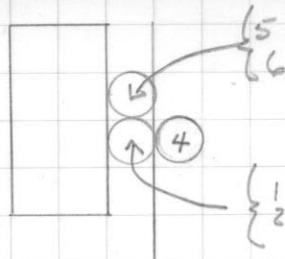
Part 001,	position - 3.5, -7, 15,	base rate	2.030×10^5
002,	-3.5, 0, 15,		2.047
004,	3.5, -7, 15,		1.990
005,	3.5, 0, 15 ,		<u>1.974</u>
		Total	8.041×10^5

T/C's on paths 001 and 004



16th Assembly (A-16)

Square tube bases



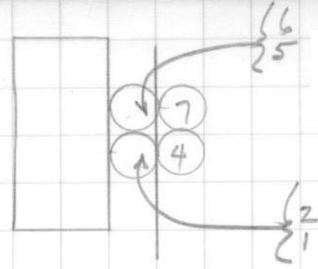
Parts 001, position -3.5, -3.5, 15-, base rate 2.030×10^5

2	-3.5, -3.5, 19.6	2.047
4	3.5, -3.5, 15-	1.990
5	-3.5, 3.5, 15-	1.974
6	-3.5, 3.5, 19.6	2.023

Total 10.064×10^5 n/sec

T/C's on #001 and 004

Table Pos cm	T-1 cts/3min	Eff Factor	n/sec $\times 10^{-5}$	M	T-2 cts/3min	Eff Factor	n/sec $\times 10^{-5}$	M
39.7 V	11455	Ave 7.64 $\times 10^6$	83.29	8.28	13300	Ave 9.24 $\times 10^6$	79.97	7.95
65.9 H								
0.14 V	11404	Ave 7.64	82.93	8.24	13568	Ave 9.24	79.41	7.89
65.9 H		T/C's #1-95°F, #2-87°F				Room - 71°F		
0.14 V	10578	Ave 7.64	76.92	7.64	12312	Ave 9.24	74.02	7.35
9.55 H		T/C's #1-95°F, #2-88°F				Room - 71°F		
0.14 V	14812	Ave 7.64	107.70	10.7	18223	Ave 9.24	109.56	10.9
0.00 H		T/C's #1-100°F, #2-87°F				Room - 71°F		

17 Assembly (A-17)

Parts 001, position -3.5, -3.5, 15, base rate 2.030×10^5 n/sec

2	-3.5, -3.5, 19.6	2.047
4	3.5, -3.5, 15	1.990
5	-3.5, 3.5, 15	1.974
6	-3.5, 3.5, 19.6	2.023
7	3.5, 3.5, 15	1.980

T/C's on 001 and 004

Table for	T-1 cm	Eff cts/3min	n/sec $\times 10^{-5}$	M	Total	12.044 $\times 10^5$ n/sec	M
					T-2 cts/3min	Eff cts/min	n/sec $\times 10^{-5}$

39.7 V 12079 Ave 7.64×10^6 87.84 7.29 14569 Ave 9.24×10^6 87.60 7.28
65.9 H

0.14V 11993 7.64 87.21 7.24 14065 9.24 84.57 7.02
65.9 H T/C's #1 - 102°F, #2 - 88°F, Room - 71°F

0.14V 12038 7.64 87.53 7.27 14323 9.24 86.11 7.15
9.55H T/C's #1 - 102°F, #2 - 89°F, Room - 71°F

0.14V
1.396H 20694 7.64 150.47 12.5 24880 9.24 149.61 12.4
T/C's #1 - 103°F, #2 - 89°F, Room - 71°F
8/19/65

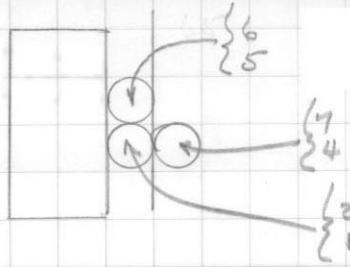
0.14V 12467 7.64 90.65 7.53 14500 9.24 87.18 7.24
9.55H T/C's #1 - 106°F, #2 - 89°F, Room - 71°F

0.14V 16262 7.64 118.25 9.83 19450 9.24 116.95 9.71
3.00H T/C's #1 - 106°F, #2 - 89°F, Room - 71°F

0.14V 20789 7.64 151.16 12.55 24868 9.24 149.52 12.41
1.392H T/C's #1 - 106°F, #2 - 89°F, Room - 71°F

0.14V 35397 7.64 257.40 21.37 41928 9.24 252.09 20.93
0.00H T/C's #1 - 106°F, #2 - 89°F, Room - 71°F

18-th Assembly (A-18)



Parts 001	, position	-3.5, -3.5, 15	, dose rate	$2.030 \times 10^5 \text{ n/sec}$
2		-3.5, -3.5, 19.6		2.047
4		3.5, -3.5, 15		1.990
5		-3.5, 3.5, 15		1.974
6		-3.5, 3.5, 19.6		2.033
7		3.5, -3.5, 19.6		1.980
			Total	$12.044 \times 10^5 \text{ n/sec}$

T/C's am 001 and 004

Table Pos	T-1 cm	Eff cts/2 min	n/sec $\times 10^{-5}$	M	T-2 cts/2 min	Eff n/sec $\times 10^{-5}$	M
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0.14V	8259	7.64	90.09	7.48	9887	9.24	89.17	7.40
65.9 H	T/C's	#1-106 °F, #2-89 °F, Room - 71 °F						

0.14V	8616	7.64	93.98	7.80	10521	9.24	94.89	7.88
9.55 H	T/C's	#1-105 °F, #2-90 °F, Room - 71 °F						

0.14V	10859	7.64	118.44	9.85	13359	9.24	120.48	10.00
4.006 H	T/C's	#1-105 °F, #2-91 °F, Room - 71 °F						

0.14V	11873	7.64	129.50	10.75	14789	9.24	133.37	11.07
3.002 H	T/C's	#1-105 °F, #2-90 °F, Room - 70 °F						

0.14V	14254	7.64	155.47	12.91	17446	9.24	157.34	13.06
2.000 H	T/C's	#1-105 °F, #2-91 °F, Room - 71 °F						

0.14V	18086	7.64	197.28	16.38	22722	9.24	204.92	17.01
1.000 H	T/C's	#1-105 °F, #2-92 °F, Room - 71 °F						

0.14 V	23489	7.46	262.39	21.79	28698	9.24	258.82	21.48
0.500 H	T/C's	#1-105 °F, #2-92 °F, Room - 71 °F						

0.14 V	32172	7.46	359.38	29.87	40315	9.24	363.57	30.19
0.000 H	T/C's	#1-106 °F, #2-93 °F, Room - 71 °F						

.18

.16

.14

.12

M-1

0.10

0.08

0.06

0.04

0.02

0.00

200 T-1:

$$\frac{\Delta k}{\Delta x} = \left| \frac{\Delta M^{-1}}{\Delta x} \right| = \frac{0.07}{2.5} = 0.030 \text{ cm}^{-1}$$

$$\approx 0.076 \text{ in}^{-1}$$

$$\frac{\Delta k}{\Delta x} \times \frac{\Delta x}{\Delta t} \times \frac{1}{f} =$$

$$\frac{0.076}{0.0019} \times 0.27 = \frac{0.021}{0.0019} = 11.05 \text{ / min}$$

$$\approx 0.18 \text{ $/sec$}$$

M = 100

9 8 7 6 5 4 3 2 1 0

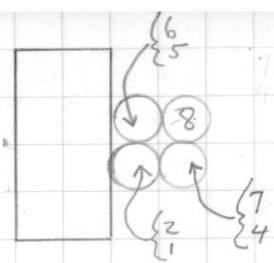
Table separation (x), cm

○ Assy A17
 △ Assy A18
 ▽ Assy A19
 ◊ Assy A19

counted T-1
 ss selected (c-1)

$$\Delta k = \Delta \left(\frac{1}{M} \right)$$

19xx Assembly (A-19)



Parts 001, position -3.5, -3.5, 15 base rate	2.030×10^5 n/sec
2	-3.5, -3.5, 19.6
4	3.5, -3.5, 15
5	-3.5, 3.5, 15
6	-3.3, 3.5, 19.6
7	3.5, -3.5, 19.6
8	3.5, 3.5, 15
	<u>2.009</u>

Total 14.053×10^5 n/sec

T/C's on 001 and 004

Table Pos cm	T-1 cts/min	Eff	n/sec $\times 10^{-5}$	M	T-2 cts/min	Eff	n/sec $\times 10^{-5}$	M
-----------------	----------------	-----	---------------------------	---	----------------	-----	---------------------------	---

39.7 V 9158 Avg 7.64×10^6 99.88 7.11 11360 Avg 9.24×10^6 102.46 7.29
65.9 H T/C's #1- $^{\circ}\text{F}$, #2- $^{\circ}\text{F}$, Room - $^{\circ}\text{F}$

0.14 V 8806 7.64 96.05 6.83 11187 9.24 100.89 7.18
65.9 H T/C's #1- 105 $^{\circ}\text{F}$, #2- 95 $^{\circ}\text{F}$, Room - 71 $^{\circ}\text{F}$

0.14 V 10219 7.64 111.47 7.93 13061 9.24 117.79 8.38
9.55 H T/C's #1- 105 $^{\circ}\text{F}$, #2- 96 $^{\circ}\text{F}$, Room - 71 $^{\circ}\text{F}$

0.14 V 12313 7.64 134.29 9.56 15712 9.24 141.70 10.08
6.001 H T/C's #1- 105 $^{\circ}\text{F}$, #2- 96 $^{\circ}\text{F}$, Room - 70 $^{\circ}\text{F}$

0.14 V 15557 7.64 169.68 12.07 20016 9.24 180.51 12.84
4.002 H T/C's #1- 105 $^{\circ}\text{F}$, #2- 97 $^{\circ}\text{F}$, Room - 70 $^{\circ}\text{F}$

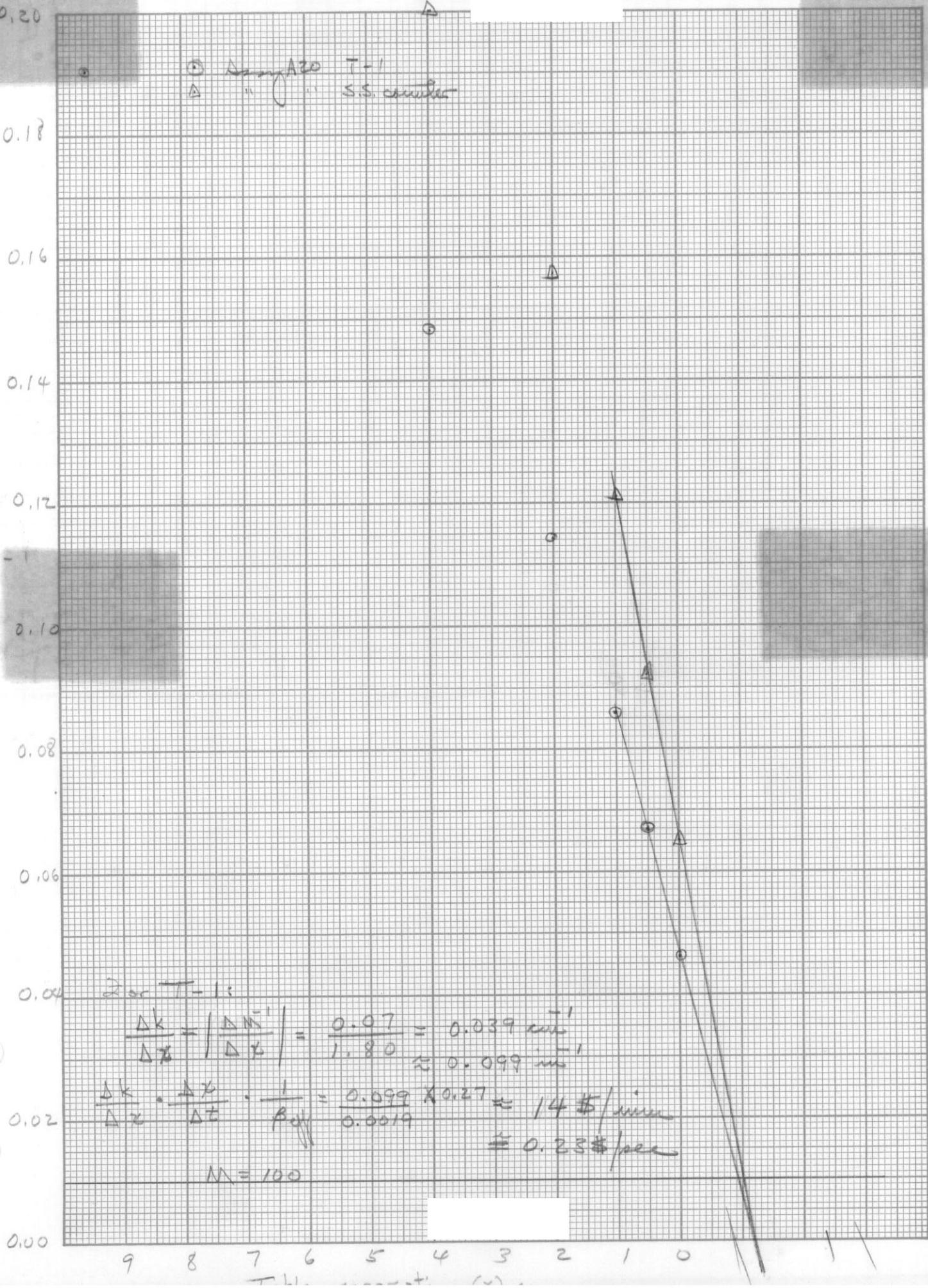
0.14 V 19111 7.64 208.12 14.81 24549 9.24 221.40 15.75
3.000 H T/C's #1- 105 $^{\circ}\text{F}$, #2- 98 $^{\circ}\text{F}$, Room - 71 $^{\circ}\text{F}$

0.14 V 27870 7.64 303.99 21.63 35619 9.24 321.23 22.86
2.003 H T/C's #1- 105 $^{\circ}\text{F}$, #2- 98 $^{\circ}\text{F}$, Room - 71 $^{\circ}\text{F}$

0.14 V 38217 7.64 416.23 29.62 48593 9.24 438.25 31.17
1.500 H T/C's #1- 105 $^{\circ}\text{F}$, #2- 98 $^{\circ}\text{F}$, Room - 71 $^{\circ}\text{F}$

Tall Pn cm	T-1 cts/2 min	Eff	$n/\text{sec} \times 10^{-5}$	M	T-2 cts/2 min	Eff	$n/\text{sec} \times 10^{-5}$	M
0.14 V	34678/1	7.64	756.49	53.83	43893/1	9.24	791.72	56.34
1.00 H	T/C's #1 - 106 °F, #2 - 98 °F, Room - 71 °F							
0.14 V	79188/1	7.64	1726.4	122.8	100982/1	9.24	1821.1	129.6
0.70 H	T/C's #1 - 105 °F, #2 - 99 °F, Room - 71 °F							
Same as above, solid-state detector mounted inside part 008. Spacers set on "in" limit switches to prevent full closure.								
0.14 V	10241	7.64	111.70	7.95	12798	9.24	115.42	8.21
9.55 H	T/C's #1 - 105 °F, #2 - 100 °F, Room - 71 °F							
	S.S. counter	4.00	619 cts (?)					
0.14 V	12395	7.64	134.93	9.60	15624	9.24	140.90	10.03
6.00 H	T/C's #1 - 104 °F, #2 - 99 °F, Room 70 °F							
	S.S. counter	4.00	557 cts					
0.14 V	15627	7.64	170.46	12.13	19738	9.24	178.00	12.67
4.000 H	T/C's #1 - 105 °F, #2 - 99 °F, Room 70 °F							
	S.S. counter	4.00	726 cts					
0.14 V	19233	7.64	209.77	14.93	24210	9.24	218.34	15.54
3.000 H	T/C's #1 - 104 °F, #2 - 99 °F, Room 70 °F							
	S.S. counter	4.00	879					
0.14 V	27051	7.64	295.05	21.00	34677	9.24	288.97	20.56
2.000 H	T/C's #1 - 104 °F, #2 - 99 °F, Room 70 °F							
	S.S. counter	4.00	1358					
0.14 V	64083	7.64	698.99	49.74	81947	9.24	739.05	52.59
1.000 H	T/C's #1 - °F, #2 - °F, Room °F							
	S.S. counter	4.00	3113					

∴ S.S. detector a little better than Tubs for M^{-1} measurement
probably; agrees very well for crit. portion.



358-10½
MADE IN U.S.A.
20 X 20 TO THE INCH
KEUFFEL & ESSER CO.

20 X 20 TO THE INCH
KEUFFEL & ESSER CO.

20th Assembly (A-20) Same as A-19 but reflector absent

Base rate $14.053 \times 10^5 \text{ n/sec}$

Table Pos cm	T-1 cts/3 min	Eff	n/sec $\times 10^{-5}$	M	T-2 cts/3 min	Eff	n/sec $\times 10^{-5}$	M
39.7 V	9427	$14.7.49 \times 10^5$	69.92	4.98	11958	Ave 9.14×10^5	72.68	5.17
65.9 H	T/C's #1 - 102°F, #2 - 99°F, Run 70°F S.S. Counter	4.00	293					
0.14 V	9033	7.49	67.00	4.77	11254	9.14	68.40	4.87
65.9 H	T/C's #1 - 101°F, #2 - 99°F, Run 70°F S.S. Counter	4.00	287					
0.14 V	9910	7.49	73.51	5.25	12809	9.14	77.86	5.54
9.55 H	T/C's #1 - 100°F, #2 - 99°F, Run 70°F S.S. Counter	4.00	365					
0.14 V	12797	7.49	94.91	6.75	16454	9.14	100.01	7.12
4.00 H	T/C's #1 - 100°F, #2 - 99°F, Run - 70°F S.S. Counter	4.00	482					
0.14 V	16612	7.49	123.21	8.77	21793	9.14	132.46	9.42
2.00 H	T/C's #1 - 100°F, #2 - 99°F, Run - 70°F S.S. Counter	4.00	635					
0.14 V	14674 1/2	7.49	163.26	11.62	19185 1/2	9.14	174.92	12.45
1.00 H	T/C's #1 - 100°F, #2 - 99°F, Run - 70°F S.S. Counter	4.00	820					
0.14 V	18892 1/2	7.49	210.18	14.96	24429 1/2	9.14	222.74	15.85
0.50 H	T/C's #1 - 100°F, #2 - 99°F, Run - 70°F S.S. Counter	4.00	1085					
0.14 V	27362 1/2	7.49	304.43	21.66	36315 1/2	9.14	331.11	23.56
0.00 H	T/C's #1 - 100°F, #2 - 98°F, Run - 70°F S.S. Counter	4.00	1530					

$$\begin{array}{r}
 0.345 \\
 + 0.027 \\
 \hline
 0.372
 \end{array}$$

0.25 mm
.195

$$\begin{array}{r}
 1.755 \\
 - 0.027 \\
 \hline
 1.728
 \end{array}$$

$$\begin{array}{r}
 2.40 \\
 - .69 \\
 \hline
 1.71
 \end{array}$$

(25-1) yellowed stone

Study of 8-Member Quasi-Cubic Array

Set up Assembly B-1: Pu to Pu initial separation 2.78 cm. (ave.)

Breakdown of lateral spacings:

2 fixed
2 fixed
Variable

$$\begin{aligned}
 \text{Can wall thickness } 0.025 \text{ cm} (0.010 \text{ in}) \times 2 &= 0.05 \text{ cm} \\
 \text{Can surface within tube } 0.32 \text{ cm} &\times 2 = 0.64 \text{ cm} \\
 \text{Tube to tube separation} &= 2.23 \text{ cm} \\
 \text{Total lateral separation} &= 2.92 \text{ cm}
 \end{aligned}$$

Vertical spacing:

Variable
Fixed
Fixed

$$\begin{aligned}
 \text{Al spacers } 0.483 \text{ cm} + 2.07 \text{ cm} &= 2.55 \text{ cm} \\
 \text{Can lid thickness } 0.020 \text{ cm} (0.008 \text{ in}) &= 0.02 \text{ cm} \\
 \text{Can bottom surface to Pu slug surface } (0.026 \text{ in}) &= 0.07 \text{ cm} \\
 \text{Total vertical spacing} &= 2.64 \text{ cm}
 \end{aligned}$$

9/2/65

Spacing of reflector control element to tube = 0.008 cm (0.003 in)
on inner limit

Part #	Position		
	x	y	z
1	-6.0	-3.5	15
2	-6.0	-3.5	22
4	3.5	-3.5	15
5	3.5	-3.5	22
6	-6.0	6.0	15
7	-6.0	6.0	22
8	3.5	6.0	15
9	3.5	6.0	15

T/C #1 in place

T/C #2 in place

16.081×10^5 n/sec = base rate

Table Pos cm	T-1 cts/4min	Eff	n/sec $\times 10^{-5}$	M	T-2 cts/4min	Eff	n/sec $\times 10^{-5}$	M
0.14 V	9592	7.5×10^{-6}	53.29	3.31	11155	9.0×10^{-6}	51.64	3.21
9.592 H S. counter								
At 15.00 T/C's #1 - 99°F, #2 - 91°F, Room 71°F								
At 0.00	9703	7.5×10^{-6}	53.91	3.35	11607	9.0×10^{-6}	53.70	3.34
<u>T/C's #1 - 99°F, #2 - 91°F, Room 71°F</u>								
0.14 V	9650/3	7.5×10^{-6}	71.48	4.44	11133/3	9.0×10^{-6}	68.72	4.27
0.00 At T/C's #1 - 100°F, #2 - 92°F, Room 71°F								
15.0 Act								
0.00 Act	9778/3	7.5×10^{-6}	72.43	4.50	11362/3	9.0×10^{-6}	70.13	4.36
<u>T/C's #1 - 101°F, #2 - 93°F, Room 71°F</u>								

Assembly B-2 Pu-to-Pu separation 2.34 cm (ave.)

Lateral spacing: 0.69 cm fixed + 1.71 cm variable = 2.40 cm

Vertical spacing: 0.57 cm fixed + 1.65 cm variable = 2.22 cm

Ave. spacing = 2.34 cm

Positions

Part #	x	y	z	
1	-3.5	-3.5	1.5	T/C in place
2	-3.5	-3.5	21.5	
4	5.0	-3.5	1.5	T/C in place
5	5.0	-3.5	21.5	
6	-3.5	5.5	1.5	
7	-3.5	5.5	21.5	
8	5.0	5.5	1.5	
9	5.0	5.5	21.5	

$$\text{Base rate} = 16.081 \times 10^5 \text{n/sec}$$

Base rate 16.081×10^5 n/sec

Position cm	T-1 cts/4mm	Eff. $\times 10^{-5}$	n/sec	M	T-2 cts/4mm	Eff. $\times 10^{-5}$	n/sec	M
0.14V	1035-6	7.5×10^{-6}	57.53	3.58	11974	9.0×10^{-6}	55.43	3.45
9.55H	S.S. Counter	$228/5 =$	45.6 c/m					
15.00A	T/C's	1 - 95°F, 2 - 94°F,	Room	71°F				
0.14V	11150/3	7.5×10^{-6}	82.59	5.14	13098/3	9.0×10^{-6}	80.86	5.03
0.00H	S.S. Counter	$223/4 =$	55.8 c/m					
15.00A	T/C's	1 - 97°F, 2 - 96°F,	Room	71°F				
0.14V	11374/3	7.5×10^{-6}	84.25	5.24	13500/3	9.0×10^{-6}	83.33	5.18
0.00H	S.S. Counter	$221/4 =$	55.2 c/m					
0.00A	T/C's	1 - 97 °F, 2 - 96 °F,	Room	71 °F				

Assembly B-3 Pu-to-Pu separation 1.74 cm

Lateral spacing: 0.69 cm fixed + 1.11 cm variable = 1.80 cm

Vertical spacing: 0.57 cm fixed + 1.05 cm variable = 1.62 cm

Position

Part #	x	y	z	
1	-3.5	-3.5	15	T/C #1 in place
2	-3.5	-3.5	21	
4	5.0	-3.5	15	T/C #2 in place
5	5.0	-3.5	21	
6	-3.5	5.0	15	
7	-3.5	5.0	21	
8	5.0	5.0	15	
9	5.0	5.0	21	

Assembly B-4

9/7/65

Counter T-1, S.S. Cr.

0.20

0.18

0.16

0.14

0.12

M-1

0.10

0.08

0.06

0.04

0.02

0.00

358-10½
MADE IN U.S.A.

20 X 20 TO THE INCH
KEUFFEL & ESSER CO.

K&E

C

C

C

C

10.0

8.0

5.0

2.0

1.0

0.0

Table Separation, cm

- Ctr T-1 Activate OUT
- ▽ " " Activate IN
- △ SS Cr Activate OUT
- ▽ SS Cr Activate IN

(Errors are counter statistics)

A

B

C

D

E

F

G

H

I

J

K

L

M

N

O

P

Q

R

S

Act. O

Act. I

Position cm	T-1			Eff $\times 10^{-5}$			T-2			Eff $\times 10^{-5}$			M
	cts/4min	n/sec	M	cts/4min	n/sec	M	cts/4min	n/sec	M	cts/4min	n/sec	M	
0.14V	11721	7.5×10^6	65.12	4.05	13381	9.0×10^6	61.94	3.85					
9.55H			S.S. Counter - $291/5 = 58.2$ c/m										
15.00 A	T/C's	#1 - 93°F.	, #2 - 92°F.										
0.14V	15676/3	7.5×10^6	116.1	7.22	18234/3	9.0×10^6	112.6	7.00					
0.00 H			S.S. Counter - $405/4 = 101$ c/m										
15.00 A	T/C's	#1 - 96°F	, #2 - 95°F										
0.14V	16057/3	7.5×10^6	118.9	7.39	18721/3	9.0×10^6	115.6	7.19					
0.00 H			S.S. Counter - $363/4 = 91$ c/m										
0.00 A	T/C's	#1 - 96°F	, #2 - 95°F										

9/7/65
Assembly B-4 Pu-to-Pu separation 1.14 cm (Ave.)

Lateral spacing: 0.69 fixed + 0.51 variable = 1.20 cm

Vertical spacing: 0.57 cm fixed + 0.45 variable = 1.02 cm

Position

Part #	x	y	z	
1	-3.5	-3.5	1.5	T/C #1 in place
2	-3.5	-3.5	22.5	
4	4.5	-3.5	1.5	
5	4.5	-3.5	22.5	T/C #2 in place
6	-3.5	4.5	1.5	
7	-3.5	4.5	22.5	
8	4.5	4.5	1.5	
9	4.5	4.5	22.5	

Assembly B-4 9/7/65 Counter T-2

0.20

0.18

0.16

0.14

M⁻¹

0.12

0.10

0.08

0.06

0.04

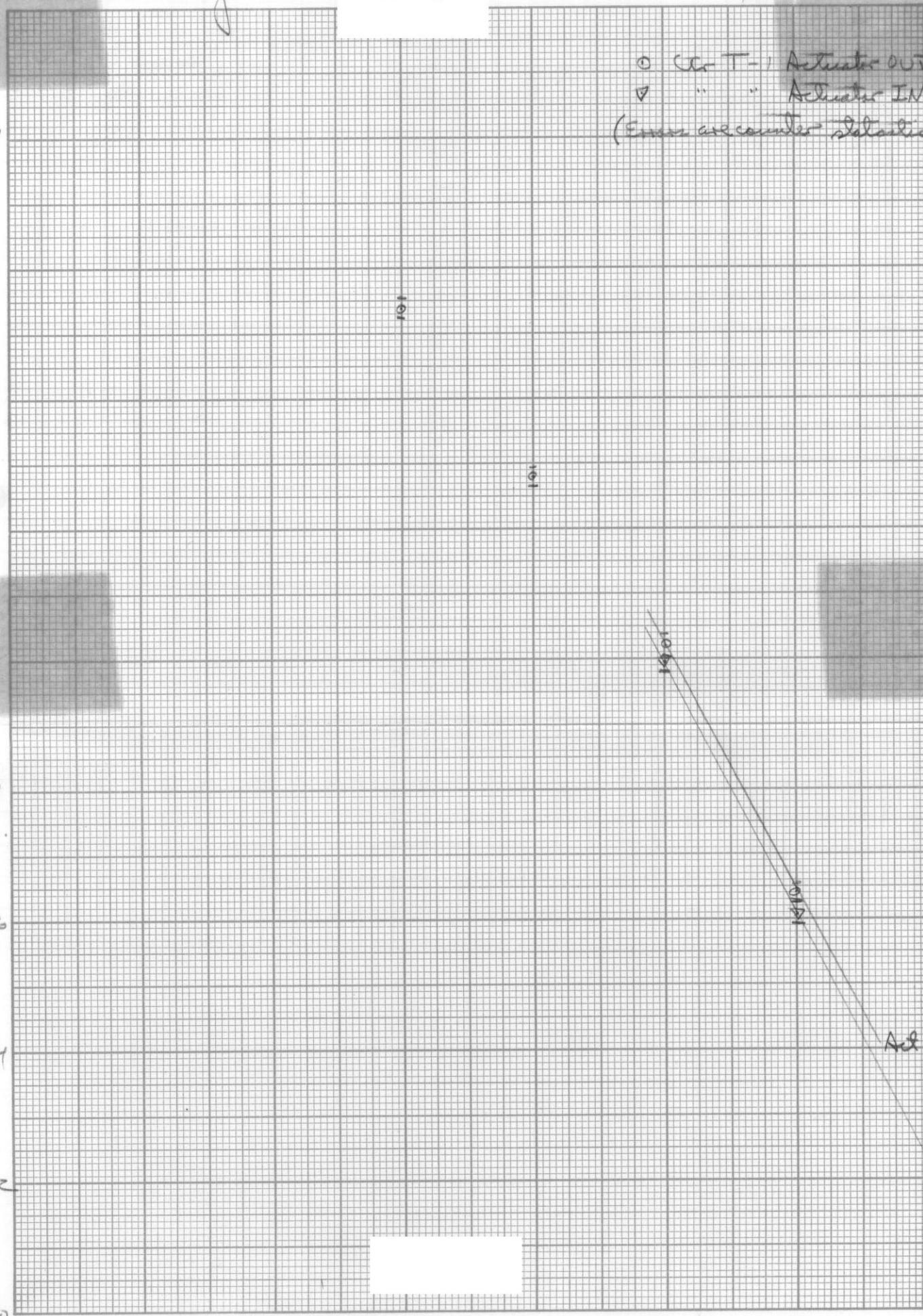
0.02

0.00

358-10½
MADE IN U.S.A.

20 X 20 TO THE INCH
KEUFFEL & ESSER CO.

K&E



Title Separation, cm

Base Rate 16.081×10^5 n/sec

Position	T-1 cm	Eff cts/min	n/sec $\times 10^{-5}$	M	T-2 cts/min	Eff n/sec $\times 10^{-5}$	M
0.14V	1065 ± 0	7.5×10^{-6}	78.89	4.91	1220.8	9.0×10^{-6}	75.36
2.00H	T/C's #1 - 92 °F, #2 - 99 °F, Room 71 °F						
15.00A	SS Counter	280 / 4.06					
0.14V	10181/2	7.5×10^{-6}	113.12	7.03	11237/2	9.0×10^{-6}	104.04
2.00H	T/C's #1 - 94 °F, #2 - 102 °F, Room 71 °F						
15.00A	SS Counter	288 / 3.00					
0.14V	11724/2	7.5×10^{-6}	130.27	8.10	13579/2	9.0×10^{-6}	125.73
2.00H	T/C's #1 - 95 °F, #2 - 103 °F, Room 71 °F						
15.00A	SS Counter	367 / 3.00					
0.14V	14929/2	7.5×10^{-6}	165.88	10.32	17085/2	9.0×10^{-6}	158.20
1.00H	T/C's #1 - 95 °F, #2 - 103 °F, Room 71 °F						
15.00A	SS Counter	414 / 3.00					
0.14V	14977/2	7.5×10^{-6}	166.41	10.35	17513/2	9.0×10^{-6}	162.15
1.00H	T/C's #1 - 96 °F, #2 - 104 °F, Room 71 °F						
0.00A	SS Counter	452 / 3.00					
0.14V	24522/2	7.5×10^{-6}	272.46	16.94	28650/2	9.0×10^{-6}	265.27
0.00H	T/C's #1 - 98 °F, #2 - 106 °F, Room 71 °F						
0.00A	SS Counter	674 / 3.00					
0.14V	23427/2	7.5×10^{-6}	260.31	16.19	27084/2	9.0×10^{-6}	250.77
0.00H	T/C's #1 - 100 °F, #2 - 106 °F, Room 71 °F						
15.00A	SS Counter	658 / 3.00					

9/7/65

Assembly B-5

U.S., T-1 and S.S.

0.20

0.18

0.16

0.14

M-1

0.12

0.10

0.08

0.06

0.04

0.02

0.00

- T-1 Actuator OUT
- △ T-1 Actuator IN
- ▽ S.S. Cls. Actuator OUT
- ◇ S.S. Cls. Actuator IN

5.0

4.0

3.0

2.0

1.0

0.0

Table Separation, cm

358-10^{1/2}
MADE IN U.S.A.20 X 20 TO THE INCH
KEUFFEL & ESSER CO.

Assembly B-5

Pw-to-Pw spacing 0.94 cm (Av.)

72

Positions

Lateral spacing: 0.69 fixed + 0.31 variable = 1.00 cm
Vertical spacing: 0.57 fixed + 0.25 variable = 0.82 cm

Part #

x

y

z

1

-3.5

-3.5

15

T/C#1 in place

2

-3.5

-3.5

22

4

4.0

-3.5

15

5

4.0

-3.5

22

T/C#2 in place

6

-3.5

4.0

15

7

-3.5

4.0

22

8

4.0

4.0

15

9

4.0

4.0

22

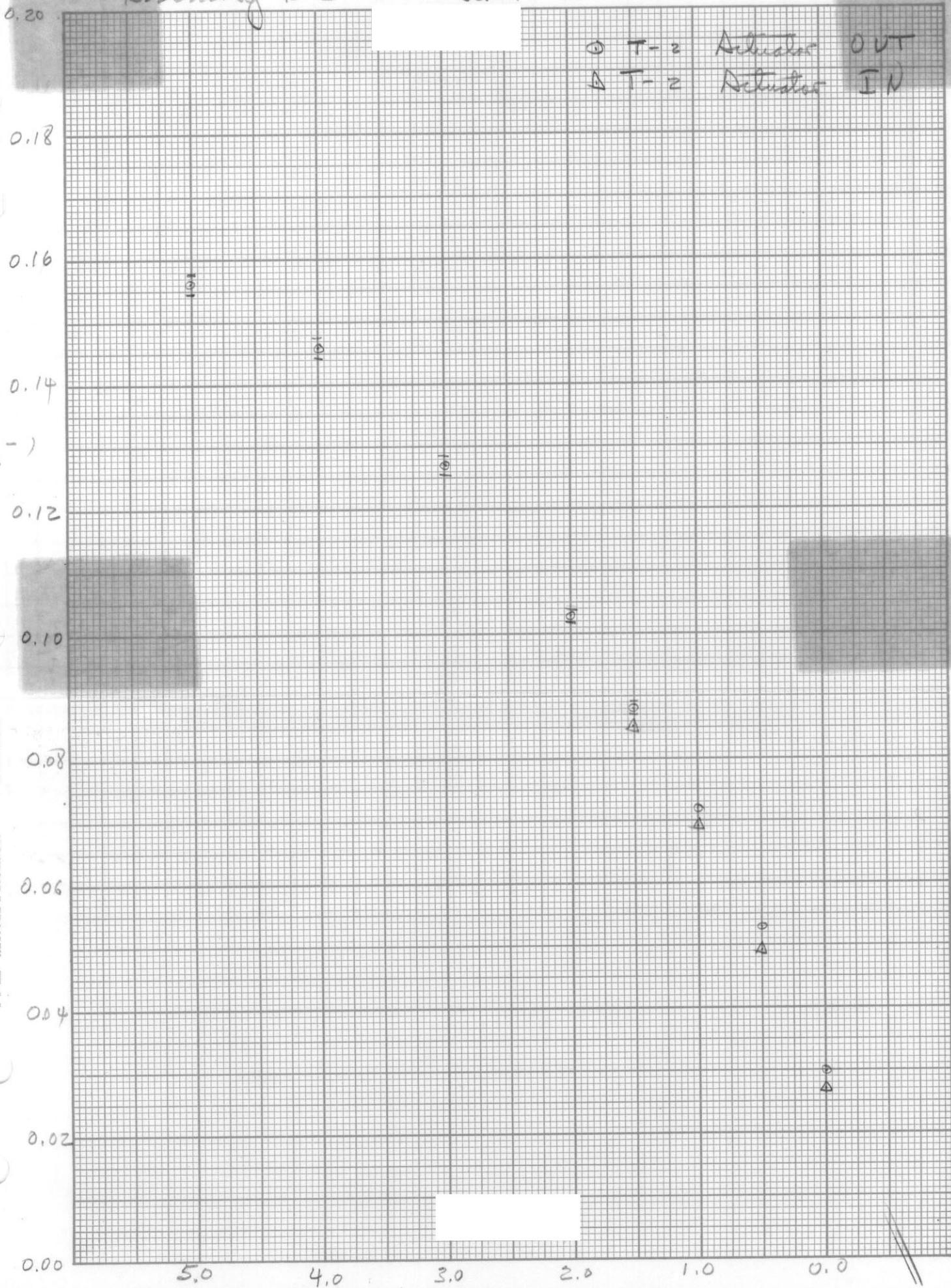
Base Rate $16.081 \times 10^5 \text{ n/sec}$

Position . cm	T-1 cts/2min	Eff	n/sec $\times 10^{-5}$	M	T-2 cts/2min	Eff	n/sec $\times 10^{-5}$	M
0.14V	11580/3	7.5×10^6	85.77	5.33	13285/3	9.0×10^6	82.01	5.10
9.55H	T/C's Room	70 °F, #1 - 95 °F, #2 - 109 °F						
15.00A	SS Counter	221/4.00						
0.14V	9645	7.5×10^6	107.16	6.66	11122	9.0×10^6	102.98	6.40
5.00H	T/C's Room	70 °F, #1 - 95 °F, #2 - 109 °F						
15.00A	SS Counter	228/3.00						
0.14V	105-26	7.5×10^6	116.96	7.27	11856	9.0×10^6	109.78	6.83
4.00H	T/C's Room	70 °F, #1 - 96 °F, #2 - 110 °F						
15.00A	SS Counter	251/3.00						
0.14V	11835	7.5×10^6	131.51	8.18	13714	9.0×10^6	126.98	7.90
3.00H	T/C's Room	70 °F, #1 - 96 °F, #2 - 110 °F						
15.00A	SS Counter	268/3.00						
0.14V	14496	7.5×10^6	161.07	10.02	16796	9.0×10^6	139.97	9.67
2.00H	T/C's Room	71 °F, #1 - 96 °F, #2 - 110 °F						
15.00A	SS Counter	330/3.00						

9/1/65

Assembly B-5

Dr T-2

358-10½
MADE IN U.S.A.20 X 20 TO THE INCH
KEUFFEL & ESSER CO.

K&E

Position cm	T-1 $\text{cts}/2\text{ min}$	Eff $\times 10^{-5}$	n/sec	M	T-2 $\text{cts}/2\text{ min}$	Eff. $\times 10^{-5}$	n/sec	M
0.14V	16978	7.5×10^6	188.64	11.73	19721	9.0×10^6	182.60	11.36
0.50H	T/C's Room	71 °F, #1 - 97 °F, #2 - 111 °F						
15.00A	SS Counter	386 / 3.00						

0.14V	21028	7.5×10^6	233.64	14.53	23990	9.0×10^6	222.13	13.82
0.50H	T/C's Room	70 °F, #1 - 97 °F, #2 - 110 °F						
15.00A	SS Counter	449 / 3.00						

0.14V	28206	7.5×10^6	313.40	19.49	32594	9.0×10^6	301.79	18.77
0.50H	T/C's Room	70 °F, #1 - 97 °F, #2 - 111 °F						
15.00A	SS Counter	637 / 3.00						

0.14V	50954	7.5×10^6	566.16	35.20	58788	9.0×10^6	544.33	33.85
0.00H	T/C's Room	70 °F, #1 - 98 °F, #2 - 112 °F						
15.00A	SS Counter	1160 / 3.00						

9/8/65-

Repeat to check normalization

0.14V	11545/3	7.5×10^6	85.52	5.32	13411/3	9.0×10^6	82.79	5.15
0.50H	T/C's Room	71 °F, #1 - 101 °F, #2 - 111 °F						
15.00A	SS Counter	231 / 4.00						

Practically identical count rates

0.14V	55921	7.5×10^6	621.35	38.64	65430	9.0×10^6	605.83	37.67
0.00H	T/C's Room	71 °F, #1 - 100 °F, #2 - 111 °F						
0.00A	SS Counter	1193 / 3.00						

0.14V	29975	7.5×10^6	333.05	20.71	35275	9.0×10^6	326.62	20.31
0.50H	T/C's same							
0.00A	SS Counter	672 / 3.00						

0.14V	21604	7.5×10^6	240.70	14.97	25346	9.0×10^6	234.69	14.59
1.00H	T/C's same							
0.00A	SS Counter	522 / 3.00						

0.14V	17511	7.5×10^6	194.56	12.10	20514	9.0×10^6	189.94	11.81
1.50H	T/C's same							
0.00A	SS Counter	386 / 3.00						

9/8/65

Assembly B-6

Cts T-1 and SS

0.20

0.18

0.16

0.14

0.12

M-1

0.10

0.08

0.06

0.04

0.02

0.00

5.0

4.0

3.0

2.0

1.0

0.0

Table Separation, cm

- T-1 Actuator OUT
 - △ T-1 Actuator IN
 - ▽ SS Counter Actuator OUT
 - ◇ SS Counter Actuator IN
- M^{-1} ml.

358-10 $\frac{1}{2}$
MADE IN U.S.A.20 X 20 TO THE INCH
KEUFFEL & SHERE CO.

K&E

C

C

Assembly B-6

Pu-to-Pu spacing 0.84 cm (Ave.)

Lateral spacing: 0.69 fixed + 0.2 variable = 0.90 cm

Vertical spacing: 0.086 fixed + 0.63 variable = 0.72 cm

Positions

Part #	x	y	z	
1	-3.5	-3.5	15	T/C #1 in place
2	-3.5	-3.5	21.5	
4	3.7	-3.5	15	
5	3.7	-3.5	21.5	T/C #2 in place
6	-3.5	3.7	15	
7	-3.5	3.7	21.5	
8	3.7	3.7	15	
9	3.7	3.7	21.5	

Base rate 16.081×10^5 n/sec

Position cm	T-1 cts/2 min	Eff	n/sec $\times 10^{-5}$	M	T-2 cts/2 min	Eff	n/sec $\times 10^{-5}$	M
0.14 V	12275/3	7.5×10^6	90.92	5.65	14328/3	9.0×10^6	88.44	57.50
9.55 H	T/C's	Room - 71 °F, #1 - 93 °F, #2 - 102 °F						
15.00 A		S.S. Counter - 262/4.00						
0.14 V	15287/3	7.5×10^6	113.24	7.04	18235/3	9.0×10^6	112.57	7.00
5.00 H	T/C's	Room - 71 °F, #1 - 96 °F, #2 - 103 °F						
15.00 A		S.S. Counter - 345/4.00						
0.14 V	11609	7.5×10^6	128.99	8.02	13487	9.0×10^6	124.88	7.77
4.00 H	T/C's	Room - 71 °F, #1 - 96 °F, #2 - 104 °F						
15.00 A		S.S. Counter - 295/3.00						
0.14 V	13439	7.5×10^6	149.32	9.29	15651	9.0×10^6	144.91	9.01
3.00 H	T/C's	Room - 71 °F, #1 - 97 °F, #2 - 105 °F						
15.00 A		S.S. Counter - 326/3.00						
0.14 V	17230	7.5×10^6	191.44	11.9	20518	9.0×10^6	189.98	11.8
2.00 H	T/C's	Room - 70 °F, #1 - 98 °F, #2 - 105 °F						
15.00 A		S.S. Counter - 456/3.00						

9/8/65 Assembly B-6

Ctr T-2

0.20

0.18

0.16

0.14

0.12

M

0.10

358-10 $\frac{1}{2}$
MADE IN U.S.A.

20 X 20 TO THE INCH
KEUFFEL & ESSER CO.

K&E

0.08

0.06

0.04

0.02

0.00

○ T-2 Actuator OUT
△ T-2 Actuator IN

5.0

4.0

3.0

2.0

1.0

0.0

Table Separation, cm

9/9/65 Assembly B-7

cts T-1 and S.S

0.20

0.18

0.16

0.14

0.12

0.10

0.08

0.06

0.04

0.02

0.00

5.0

4.0

3.0

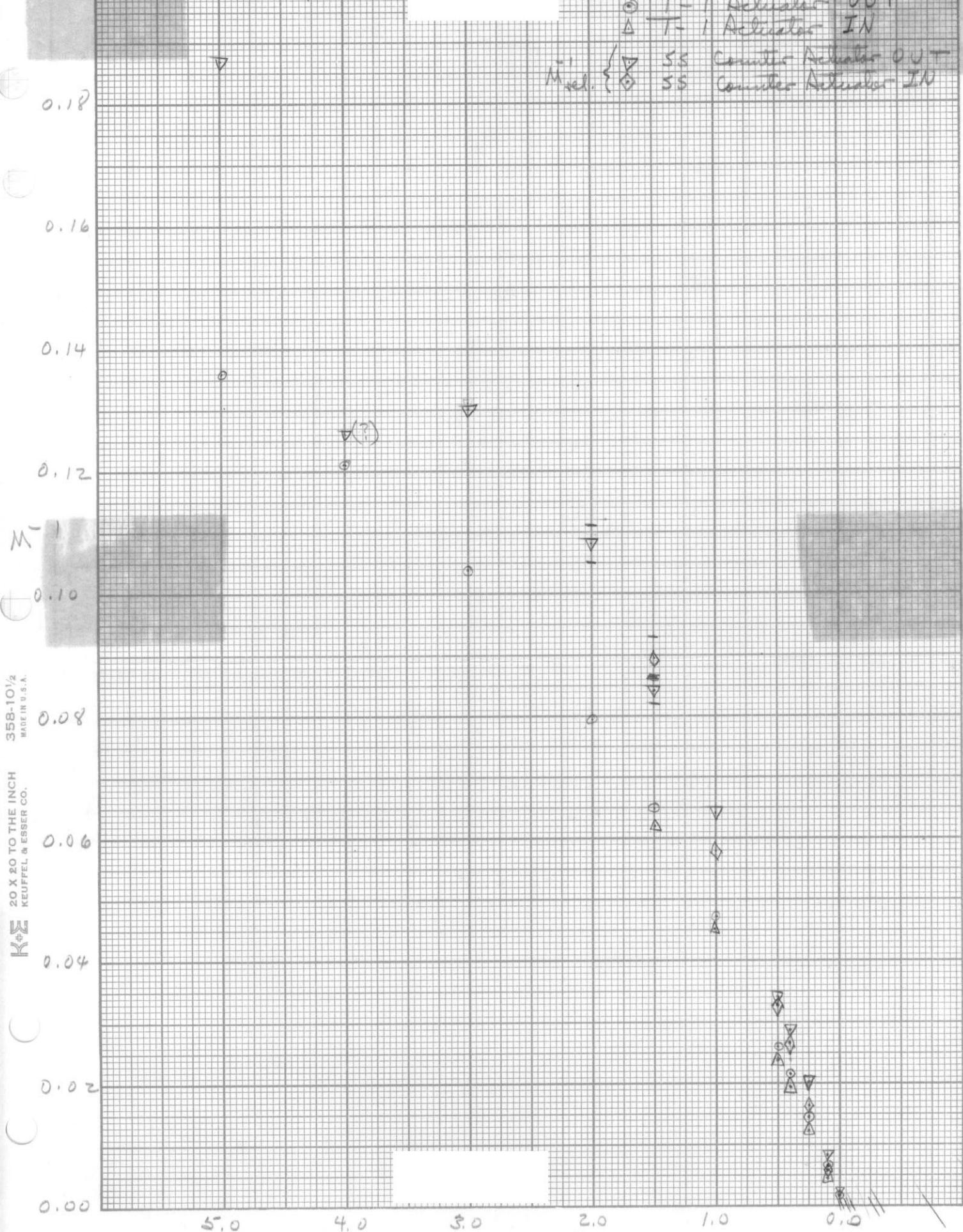
2.0

1.0

0.0

Table Separation, cm

○ T-1 Actuator OUT
△ T-1 Actuator IN
▽ SS Com��e Actuator OUT
◇ SS Com��e Actuator IN



358-10^{1/2}
MADE IN U.S.A.

20 X 20 TO THE INCH
KEUFFEL & ESSER CO.

KCC

Position cm	T-1 cts/2 min	Eff	n/sec $\times 10^{-5}$	M	T-2 cts/2 min	Eff	n/sec $\times 10^{-5}$	M
0.14U	171737	7.5×10^6	1908	118.7	194788	9.0×10^6	1803	112.1
0.00H	T/C's Room - 70 °F, #1 - 104 °F, #2 - 109 °F							
15.00A	S. S. Counter - 3952/3.00							

Assembly B-7

Pu-to-Pu spacing 0.79 cm (Av)

Lateral spacing: 0.69 fixed + 0.16 variable = 0.85 cm

Vertical spacing: 0.086 fixed + 0.59 variable = 0.67 cm

Positions

Part #	x	y	z	
1	-3.5	-3.5	15	T/C #1
2	-3.5	-3.5	21	
4	3.5	-3.5	15	
5	3.5	-3.5	21	T/C #2
6	-3.5	3.5	15	
7	-3.5	3.5	21	
8	3.5	3.5	15	
9	3.5	3.5	21	

Base rate 16.081×10^5 n/sec

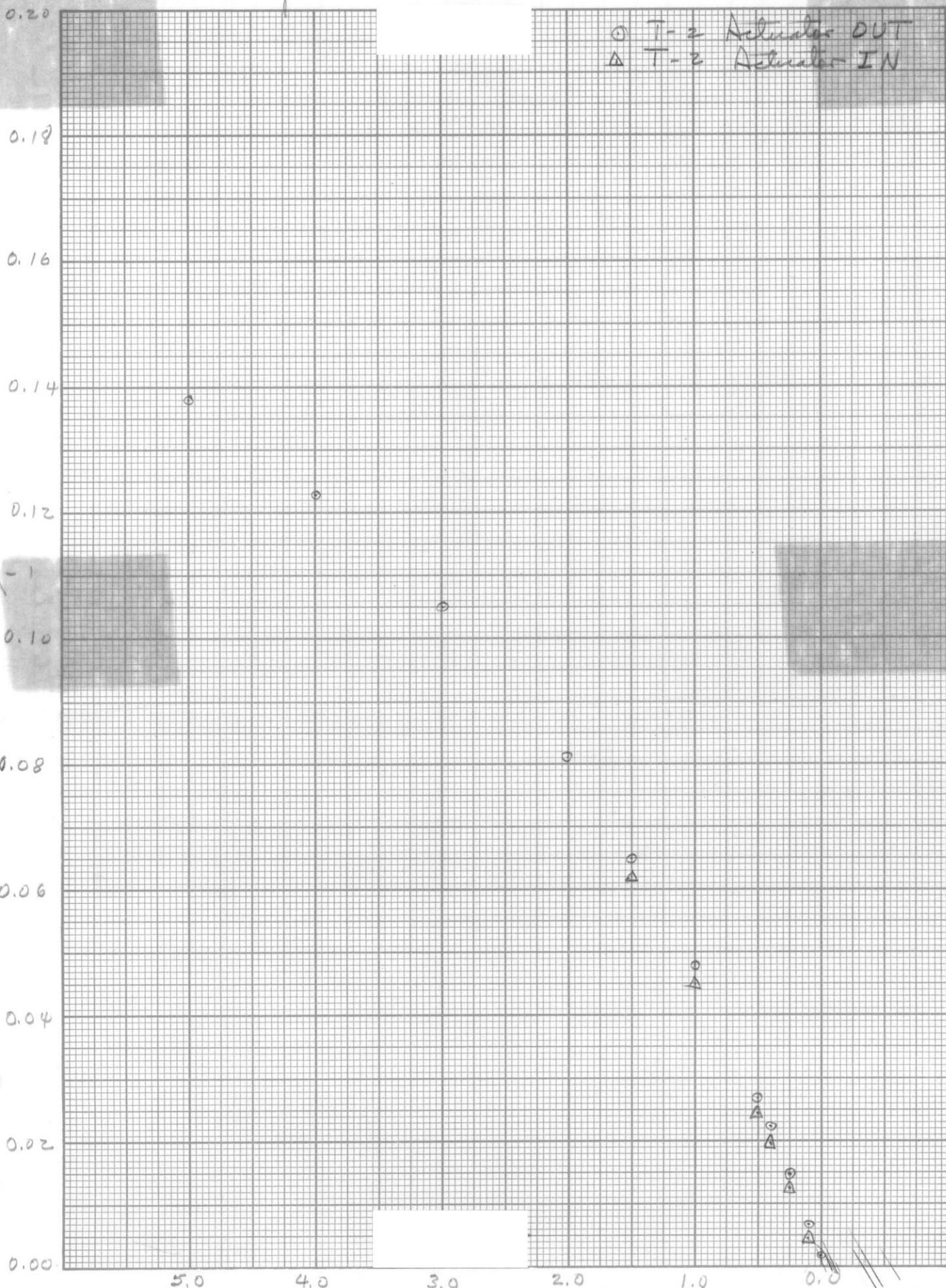
0.14U	8329	7.5×10^6	92.55	5.76	9817	9.0×10^6	90.90	5.65
9.55H	T/C's Room - 70 °F, #1 - 102 °F, #2 - 111 °F							
15.00A	S. S. Counter - 236/3.00							

0.14U	10641	7.5×10^6	118.24	7.35	12559	9.0×10^6	116.29	7.23
9.00H	T/C's Room - 71 °F, #1 - 104 °F, #2 - 112 °F							
15.00A	S. S. Counter - 268/3.00							

0.14U	11972	7.5×10^6	135.03	8.27	14101	9.0×10^6	130.57	8.12
4.00H	T/C's Room - 70 °F, #1 - 104 °F, #2 - 112 °F							
15.00A	S. S. Counter - 396/3.00 (?)							

9/9/65 Assembly B-7

Ctr. T-2



358-10^{1/2}
MADE IN U.S.A.

20 X 20 TO THE INCH
KEUFFEL & ESSER CO.



Table Separation, cm

Position cm	T-1 cts/2 min	Eff n/sec $\times 10^{-5}$	M	T-2 cts/2 min	Eff n/sec $\times 10^{-5}$	M
0.14V 3.00H 15.00A	13947 T/c's Room S.S. Counter	7.5×10^6 154.97 202.33	154.97 12.58	16608 #1 - 104°F, #2 - 112°F S.S. Counter - 386/3.00	9.0×10^6 153.77	9.56
0.14V 2.00H 15.00A	18210 T/c's Room S.S. Counter	7.5×10^6 71°F, #1 - 104°F, #2 - 112°F S.S. Counter - 459/3.00	202.33 12.58	21540	9.0×10^6 199.44	12.40
0.14V 1.50H 15.00A	22302 T/c's Room S.S. Counter	7.5×10^6 71°F, #1 - 104°F, #2 - 112°F S.S. Counter - 594/3.00	247.80 15.41	26621	9.0×10^6	15.33
0.14V 1.50H 0.00A	23367 T/c's Room S.S. Counter	7.5×10^6 71°F, #1 - 105°F, #2 - 113°F S.S. Counter - 559/3.00 (?)	259.63 16.15	27940	9.0×10^6 258.70	16.10
0.14V 1.00H 15.00A	32026 T/c's Room S.S. Counter	7.5×10^6 71°F, #1 - 105°F, #2 - 113°F S.S. Counter - 778/3.00	355.84 22.13	38843	9.0×10^6 359.65	22.36
0.14V 0.50H 0.00A	55118 T/c's Room S.S. Counter	7.5×10^6 612.41 #1 - 105°F, #2 - 113°F S.S. Counter - 1464/3.00	38.08 41.79	64770	9.0×10^6 599.72	37.29
0.14V 0.50H 0.00A	60478 T/c's Room S.S. Counter	7.5×10^6 671.97 #1 - 105°F, #2 - 113°F S.S. Counter - 1516/3.00	671.97 41.79	71498	9.0×10^6 662.02	41.17
0.14V 0.40H 15.00A	66904 T/c's Room S.S. Counter	7.5×10^6 743.37 #1 - 105°F, #2 - 113°F S.S. Counter - 1738/3.00	46.26 77977	9.0 $\times 10^6$ 722.01	44.90	
0.14V 0.40H 0.00A	74303 T/c's Room S.S. Counter	7.5×10^6 825.58 #1 - 105°F, #2 - 113°F S.S. Counter - 1657/3.00	51.34 87355	9.0×10^6 808.84	50.30	

0.14V 792506 7.5×10^{-6} 8805.61 577.58 888387 9.0×10^{-6} 8225.80 511.53
0.00 T/C's : Room 71°F #1 - 105°F #2 - 113°F
15.00 S.S. Counter - 21377 / 3.00

Repeat same on 9/10/65

0.14V 830671 7.5×10^{-6} 9229.66 573.95 945433 9.0×10^{-6} 8754.00 544.37
0.00
15.00 S.S. Counter 21790 / 3.00

Ave mult. = 55.9

Position cm	T-1 cts/2min	Eff. $n/sec \times 10^{-5}$	M	T-2 cts/2min	Eff. $n/sec \times 10^{-5}$	M
0.14V	99907	7.5×10^6	1110.08	69.03	116295×10^6	1076.80
0.25	T/C's : Room		$71^\circ F$	# 1 - $105^\circ F$	# 2 - $113^\circ F$	
15.00A			S.S. Counter	- 2990 / 3.00		
0.14V	118794	7.5×10^6	1319.93	82.08	139198×10^6	1288.86
0.25	T/C's : Room		$71^\circ F$	# 1 - $105^\circ F$	# 2 - $113^\circ F$	
0.00A			S.S. Counter	- 3082 / 3.00		
0.14V	225132	7.5×10^6	2501.46	153.55	256037×10^6	2370.71
0.10	T/C's : Room		$71^\circ F$	# 1 - $105^\circ F$	# 2 - $113^\circ F$	
15.00A			S.S. Counter	- 6175 / 3.00		
0.14V	335930	7.5×10^6	3732.54	232.11	385445×10^6	3568.93
0.10	T/C's : Room		$71^\circ F$	# 1 - $105^\circ F$	# 2 - $113^\circ F$	
0.00A			S.S. Counter	- 8740 / 3.00		

At closure CRM's were overflowed, but still was level - no persisting period.

9/10/65

Rechecked count rate at last stop to verify uniformity

0.14V 12817/3
 9.55H T/C's R - $72^\circ F$ # 1 - $106^\circ F$ # 2 - $113^\circ F$
 15.00A S. S. Counter - 282 / 4.00

Same as previously

0.14V 830671 7.5×10^6 9229.66 573.95 945433 9.0×10^{-6} 8759.00 549.37
 0.00 T/C's R - $72^\circ F$ # 1 - $106^\circ F$ # 2 - $113^\circ F$
 15.00A S. S. Counter - 21790 / 3.00

0.14V 7.5×10^{-6} 9.0×10^{-6}
 0.00 T/C's R - $72^\circ F$ # 1 - $106^\circ F$ # 2 - $113^\circ F$
 0.00A S. S. Counter - / 3.00

did not get actuator fully in.

$$\text{Period: } \frac{Q_1}{Q_0} = e^{\alpha t}$$

$$\ln \frac{Q_1}{Q_0} = \alpha t$$

$$t = \frac{1}{\alpha} \ln \frac{Q_1}{Q_0}$$

for period $\tau = t$, $\ln \frac{Q_1}{Q_0} = \ln e = 1.00$

$$\text{hence } \tau = \frac{1}{\alpha}$$

or 1.5 fold time

$$t = \frac{1}{\alpha} \ln 1.5 = \frac{1}{0.405} (0.405) = 176.5 \text{ sec}$$

$$\frac{\tau}{t} = \frac{\frac{1}{\alpha}}{\frac{1}{\alpha} \ln \frac{Q_1}{Q_0}} = \frac{1}{\ln \frac{Q_1}{Q_0}}$$

$$\tau = \frac{t}{\ln \frac{Q_1}{Q_0}} = \frac{176.5 \text{ sec}}{0.405} = 435.8 \text{ sec}$$

≈ 3.1 f reactivity

At rod position 0.495 cm we got an period which persisted:

Checked with stopwatch 1.5-fold time was 176.5 sec.
hence doubling time was 352 sec.

Then the period (e -fold) was $435.8 \text{ sec} \approx 3.1 \text{ f reactivity}$

Flux level mostly on 10×10^{-9} amps scale; at this level steady state was obtained with actuator set at 0.540 cm

Re-checked that the same period above could be achieved by going back to 0.500 cm. It confirmed. Then ran in the actuator to obtain faster periods as indicated on the period meter.

Actuator Pos. cm	Period (msec) sec	Beds 1	Beds 2	Victoreen, RAMS, f/hr				
		10^{-8} amps	10^{-8} amps	1	2	3	4	5
0.17	100.	1.7	5.0	0.1	10	0.2	0.3	2
0.10	70-80	1.7	5.0	0.3	20	0.22	0.5	2

Apparently a minimum spacing of 0.10 cm will provide an adequate amount of excess reactivity for power control. We should probably move the actuator back to limit the approach to that amount.

Re-checked initial position at level of 0.6×10^{-7} amps on Beckman 1: 0.47 cm. Looks like old problem of presence of source (Then there is a 4.2% error due to presence of source at $\sim 10^{-9}$ amps)

From single period calibration above, we get worth of actuated motion:

$$\Delta P / \Delta x \left(10 \times 10^{-9} \text{ amp scale} \right) 3.1 f / 0.045 \text{ cm} \approx 69 f / \text{cm}$$

During entire sequence maximum temperatures were Room 71°F , #1 - 105°F , #2 - 114°F .

Discovered that vertical spacing was actually 0.18 cm less than was believed - error in figuring the components in the vertical dimensions on p 67. This error was present in assemblies B-1 thru 7. Corrected in all previous notes. The following assemblies will be isotropic.

9/9/65 Assembly B-7 Ctrs T-1 and SS (Larger scale)

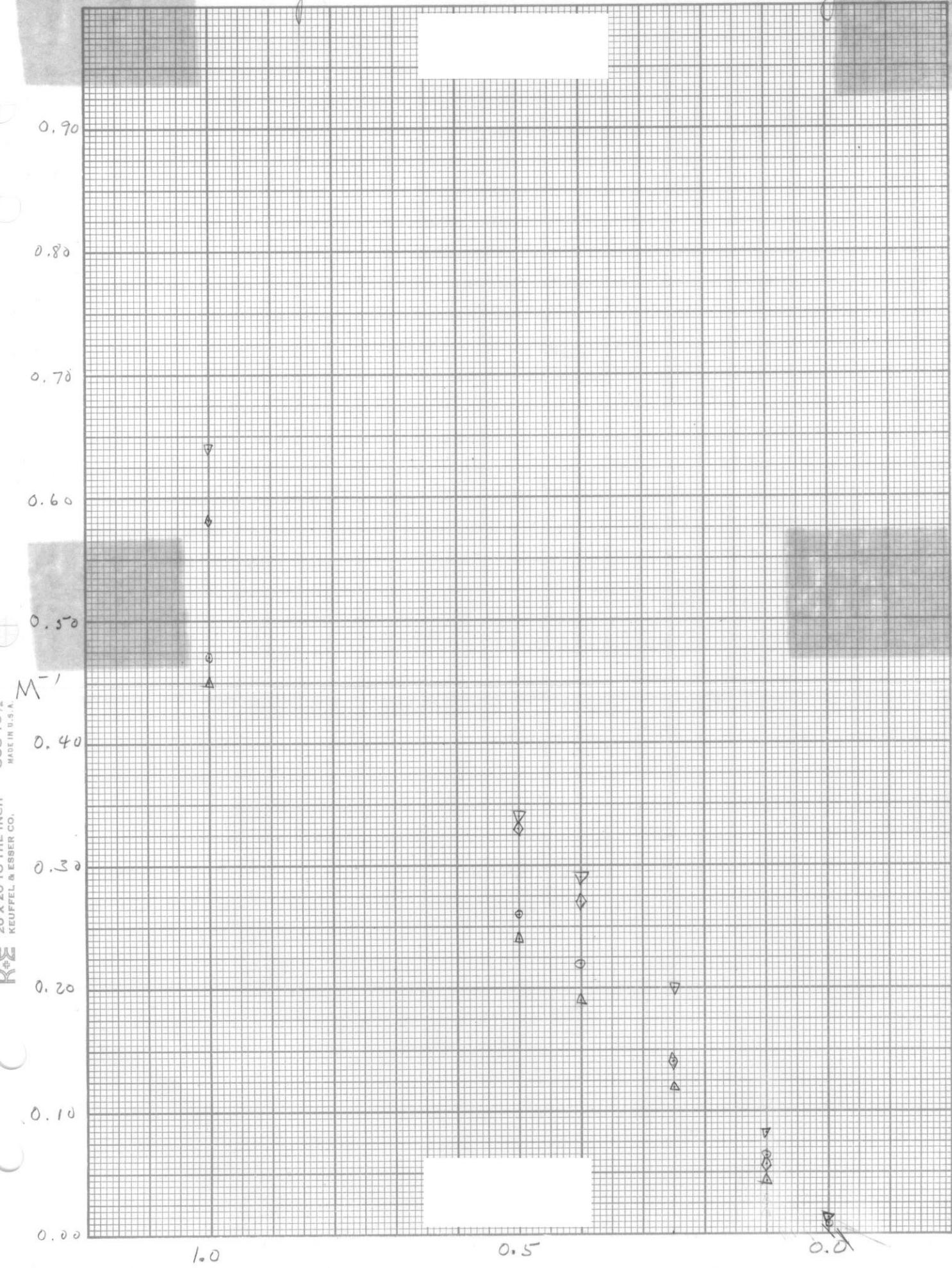


Table Separation, cm

Assembly B-8

Pu-to-Pu spacing 0.85 cm

80

Lateral spacing: 0.69 fixed + 0.16 variable = 0.85 cm

Vertical spacing: 0.086 fixed + 0.765 variable = 0.851 cm

Positions: Essentially as shown for Assembly B-7. T/c's on
part #1 and 5.

Base rate 16.081×10^5 n/sec

Position	T-1 cm	Eff cts/2 min	n/sec $\times 10^{-5}$	M	T-2 cts/2 min	Eff n/sec $\times 10^{-5}$	M
----------	-----------	------------------	---------------------------	---	------------------	----------------------------------	---

0.14V	11817/3	7.5×10^6	87.53	5.44	12646/3	9×10^{-6}	78.01	4.85
9.55H	T/C's	Room - $70^\circ F$	#1 - $98^\circ F$, #2 - $99^\circ F$					
15.00 A		S.S. Counter	-					

0.14V	9709	7.5×10^6	107.88	6.71	10522	9.0×10^{-6}	97.42	6.06
5.00H	T/C's	Room - $70^\circ F$	#1 - $100^\circ F$, #2 - $100^\circ F$					
15.00 A		S.S. Counter	-					

0.14V	10842	7.5×10^6	120.47	7.49	11516	9.0×10^{-6}	106.63	6.63
5.00H	T/C's	Room - $70^\circ F$	#1 - $101^\circ F$, #2 - $101^\circ F$					
15.00 A		S.S. Counter	-					

0.14V	12476	7.5×10^6	138.63	8.62	13492	9.0×10^{-6}	124.92	7.77
5.00H	T/C's	Room - $70^\circ F$	#1 - $102^\circ F$, #2 - $101^\circ F$					
15.00 A		S.S. Counter	-					

0.14V	15850	7.5×10^6	176.11	10.95	16924	9.0×10^{-6}	156.70	9.74
5.00H	T/C's	Room - $70^\circ F$	#1 - $102^\circ F$, #2 - $104^\circ F$					
15.00 A		S.S. Counter	- 290/3.00					

0.14V	24090	7.5×10^6	207.67	16.65	26248	9.0×10^{-6}	243.03	15.11
5.00H	T/C's	Room - $70^\circ F$	#1 - $102^\circ F$, #2 - $105^\circ F$					
15.00 A		S.S. Counter	- 469/3.00					

0.14V	102400	7.5×10^6	1137.77	70.70	108666	9.0×10^{-6}	1006.17	62.57
5.00H	T/C's	Room - $70^\circ F$	#1 - $103^\circ F$, #2 - $105^\circ F$					
15.00 A		S.S. Counter	- 1965/3.00					

Assembly B-8

9/13/65

Cts T-1 and SS

0.20

0.18

0.16

0.14

0.12

M-1
0.10

0.08

0.06

0.04

0.02

0.00

5

4

3

2

1

0

Table Separation, cm

358-10½
MADE IN U.S.A.

K&E 20 X 20 TO THE INCH
KEUFFEL & ESSER CO.

M-1
rel.

- ◎ T-1 Actuator OUT
- △ T-1 Actuator IN
- { ▽ SS Cts Actuator OUT
- { ◇ SS Cts Actuator IN

▽

▽

▽

◇

◇

△

▽

◇

Position cm	T-1 cts/2 min	Eff $\times 10^{-5}$	n/sec $\times 10^{-5}$	M	T-2 cts/2 min	Eff. $\times 10^{-5}$	n/sec $\times 10^{-5}$	M
0.140	122519	7.5×10^6	1361.3	84.65	129299	9.0×10^6	1197.21	74.45
0.00H	T/C's	#1 - 104, #2 - 105, Room - 70 °F						
0.00A	S.S. Counter	- 2099/3.00						

0.140	25762	7.5×10^6	286.24	17.80	27571	9.0×10^6	255.28	15.87
1.00H	T/C's	Room 70 °F, #1 - 105 °F, #2 - 107 °F						
0.00A	S.S. Counter	- 704/3.00						

Assembly B-9: Pu - to - Pu distance 0.80 cm

Lateral spacing: 0.69 fixed + 0.11 variable = 0.80 cm

Vertical spacing: 0.086 fixed + 0.714 variable = 0.80 cm

Positions essentially as before. T/C's on parts #1 and #5.

0.140	8208	7.5×10^6	91.20	5.67	8428	9.0×10^6	78.03	4.85-
9.55H	T/C's	Room - 70 °F, #1 - 105 °F, #2 - 107 °F						
15.00A	S. S. Counter	- 293/3.00						

0.140	10316	7.5×10^6	114.63	7.13	10712	9.0×10^6	99.19	6.17
5.00H	T/C's	Room - 70 °F, #1 - 104 °F, #2 - 107 °F						
15.00A	S. S. Counter	- 354/3.00						

0.140	11426	7.5×10^6	126.96	7.90	11704	9.0×10^6	108.37	6.74
4.00H	T/C's	Room - 70 °F, #1 - 104 °F, #2 - 106 °F						
15.00A	S. S. Counter	- 393/3.00						

0.140	13472	7.5×10^6	149.69	9.31	13678	9.0×10^6	126.64	7.88
3.00H	T/C's	Room - 70 °F, #1 - 104 °F, #2 - 107 °F						
15.00A	S. S. Counter	- 454/3.00						

0.140		7.5×10^6		11.72		9.0×10^6		10.23
2.00H	T/C's	Room - 70 °F, #1 - 104 °F, #2 - 107 °F						
15.00A	S. S. Counter	-						

Assembly B-8

9/13/65

Ch T-2

0.20

0.18

0.16

0.14

0.12

M-1

0.10

0.08

0.06

0.04

0.02

0.00

○

△

Actuator OUT
Actuator IN

358-10½
MADE IN U.S.A.

20 X 20 TO THE INCH
KEUFFEL & LESSER CO.

K&L

5.0

4.0

3.

2

1

0

Table Separation, cm

Position in	T-1 cts/2 min	Eff $\times 10^{-5}$	n/sec $\times 10^{-5}$	M	T-2 cts/2 min	Eff. $\times 10^{-6}$	n/sec $\times 10^{-5}$
0.140	20657	7.5×10^{-6}	229.52	14.27	21161	9.0×10^{-6}	195.93
1.50H	T/C's Room - 70 °F, #1 - 104 °F, #2 - 107 °F						
15.00A	SS Counter - 647/3.00						
0.140	21390	7.5×10^{-6}	237.67	14.78	22194	9.0×10^{-6}	205.50
1.50H	T/C's Room - 70 °F, #1 - 104 °F, #2 - 107 °F						
0.00A	SS Counter - 691/3.00						
0.140	27177	7.5×10^{-6}	301.97	18.78	27867	9.0×10^{-6}	258.03
1.00H	T/C's Room - 70 °F, #1 - 104 °F, #2 - 107 °F						
15.00A	SS Counter - 2211(?) / 3.00						
0.14V	28194	7.5×10^{-6}	313.27	19.48	29308	9.0×10^{-6}	271.37
1.00H	T/C's Room - 70 °F, #1 - 105 °F, #2 - 107 °F						
0.00A	SS Counter - 884/3.00						
0.14V	43608	7.5×10^{-6}	484.53	30.12	44370	9×10^{-6}	410.83
0.50H	T/C's Room - 70 °F, #1 - 105 °F, #2 - 107 °F						
15.00A	SS Counter 1289/3.00						
0.14V	47167	7.5×10^{-6}	524.08	32.59	47953	9.0×10^{-6}	444.01
0.50H	T/C's Room - 70 °F, #1 - 105 °F, #2 - 108 °F						
0.00A	SS Counter 1584/3.00						
0.14V	176211	7.5×10^{-6}	1957.89	122.37	175715	9.0×10^{-6}	1626.98
0.00H	T/C's Room - 70 °F #1 - 105 °F #2 - 108 °F						
15.00A	SS Counter - 5197/3.00						
0.14V	240194	7.5×10^{-6}	2668.61	165.96	240769	9.0×10^{-6}	2229.33
0.00H	T/C's Room - 70 °F #1 - 106 °F #2 - 108 °F						
0.00A	SS Counter 7674/3.00						

Attempted some Rossi- α measurements here - the count rates were still much too low.

Assembly B-9

Ctr T-1 and S.S. 9/14/65

0.20

0.18

0.16

0.14

0.12

M-1

0.10

358-10^{1/2}
MADE IN U.S.A.

K&K
20 X 20 TO THE INCH
KEUFFEL & ESSER CO.

0.08

0.06

0.04

0.02

0.00

- T-1 Actuator OUT
- △ T-1 Actuator IN
- ▽ S.S. Actuator OUT
- ◇ S.S. Actuator IN

5

4

3

2

1

0

Table Separation, cm

Assembly B-10: Pu-to-Pu spacing 0.725 cm

Lateral spacing: 0.69 fixed + 0.035 variable = 0.725 cm.

Vertical spacing: 0.086 fixed + 0.64 variable = 0.726 cm.

Positions: Essentially same as before; T/C's on #1 and #5

Base rate 16.081×10^{-5} n/sec

Position cm	T-1 cts/2 min	Eff	n/sec $\times 10^{-5}$	M	T-2 cts/2 min	Eff	n/sec $\times 10^{-5}$	M
0.140	12675/3	7.5×10^{-6}	93.89	5.84	13481/3	9.0×10^{-6}	83.20	5.17
9.55H	T/C's Room - 70 °F, #1-109 °F, #2-107 °F							
15.00A	S.S. Counter - 354/4.00							
0.140	10816	7.5×10^{-6}	120.17	7.48	11409	9.0×10^{-6}	105.64	6.57
5.00H	T/C's Room - 70 °F, #1-110 °F, #2-108 °F							
15.00A	S.S. Counter - 325/3.00							
0.140	12533	7.5×10^{-6}	139.25	8.66	12904	9.0×10^{-6}	119.48	7.43
4.00H	T/C's Room - 70 °F, #1-110 °F, #2-108 °F							
15.00A	S.S. Counter - 415/3.00							
0.140	14578	7.5×10^{-6}	161.97	10.07	15465	9.0×10^{-6}	143.20	8.90
3.00H	T/C's Room - 70 °F, #1-110 °F, #2-108 °F							
15.00A	S.S. Counter - X							
0.140	19624	7.5×10^{-6}	163.53	13.56	20610	9.0×10^{-6}	190.83	11.87
2.00H	T/C's Room - 70 °F, #1-110 °F, #2-108 °F							
15.00A	S.S. Counter - 646/3.00							
0.140	24474	7.5×10^{-5}	271.93	16.91	25760	9.0×10^{-6}	238.52	14.83
1.50H	T/C's Room - 70 °F, #1-111 °F, #2-108 °F							
15.00A	S.S. Counter - 781/3.00							
0.140	25861	7.5×10^{-5}	287.34	17.87	26930	9.0×10^{-6}	249.35	15.57
1.50H	T/C's Room - 70 °F, #1-110 °F, #2-109 °F							
0.00A	S.S. Counter - 829/3.00							

Assembly B-9

Ctr T-2

9/14/65

0.20

0.18

0.16

0.14

0.12

M-1

0.10

358-10 1/2
MADE IN U.S.A.

K-E 20 X 20 TO THE INCH
KEUFFEL & ESSER CO.

0.08

0.06

0.04

0.02

0.00

○ T-2 Actuator OUT
△ T-2 Actuator IN

5

4

3

2

1

0

1 1 1

Table Separation, cm

Position cm	T-1 cts/2 min.	Eff $\times 10^{-5}$	n/sec $\times 10^5$	M	T-2 cts/2 min.	Eff $\times 10^{-5}$	n/sec $\times 10^5$	M	84
0.140	35630	7.5×10^{-6}	395.89	24.62	37172	9×10^{-6}	344.19	21.40	
1.00H	T/C's	Room - 70 °F	#1 - 110 °F, #2 - 108 °F						
15.00A		S.S. Counter	- 1175 / 3.00						
0.14V	37770	7.5×10^{-6}	419.67	26.10	39502	9×10^{-6}	3655.46	22.74	
1.00H	T/C's	Room - 70 °F, #1 - 110 °F, #2 - 108 °F							
0.00A		S.S. Counter	- 1224 / 3.00						
0.14V	75349	7.5×10^{-6}	837.21	52.06	78879	9×10^{-6}	730.37	45.42	
0.50H	T/C's	Room - 70 °F, #1 - 111 °F, #2 - 109 °F							
15.00A		S.S. Counter	- 2489 / 3.00						
0.14U	85963	7.5×10^{-6}	955.15	59.40	89580	9×10^{-6}	829.44	51.58	
0.50H	T/C's	Room - 70 °F, #1 - 111 °F, #2 - 109 °F							
0.00A		S.S. Counter	- 2688 / 3.00						
0.14U	156507	7.5×10^{-6}	1738.97	108.14	158276	9×10^{-6}	1465.51	91.13	
0.30H	T/C's	Room - 70 °F, #1 - 111 °F, #2 - 109 °F							
15.00A		S.S. Counter	- 4936 / 3.00						
0.14W	203659	7.5×10^{-6}	2263.86	140.78	208134	9×10^{-6}	1927.17	119.84	
0.30H	T/C's	Room - 70 °F, #1 - 111 °F, #2 - 109 °F							
0.00A		S.S. Counter	- 6571 / 3.00						
0.14V	345734	7.5×10^{-6}	3841.48	238.88	345.574	9×10^{-6}	3199.76	198.98	
0.20H	T/C's	Room - 70 °F, #1 - 111 °F, #2 - 109 °F							
15.00A		S.S. Counter	- 11251 / 3.00						

Went to int. at 8.00A, ~ 0.128 H, w/ 400 sec period

Deduce critical spacing by interpolation of plot of lattice spacing versus extrapolated critical separation as near int as possible

Assembly	Lattice Spacing cm	Critical Table Separation cm
B-8	0.85	+0.32
B-9	0.80	+0.18
B-10	0.725	-0.10

Assembly B-10

9/15/65

Ctr T-1 and SS

0.20

0.18

0.16

0.14

0.12

M-1

0.10

0.08

0.06

0.04

0.02

0.00

① T-1 Actuator OUT
△ T-1 " IN
▽ S.S. Out " OUT
◊ S.S. Out " IN

5

4

3

2

1

0

Table Separation .cm

358-10½
MADE IN U.S.A.

K-E 20 X 20 TO THE INCH
KEUFFEL & LESSER CO.

K-E

C

C

9/17/65

Starting temperatures Room - 70°F
 #1 - 104°F
 #2 - 109°F

Started up with actuator at 2.00 cm

Went to about int with Diving-table motion, to 0.152 cm

Set up positive period with actuator at 0.730 cm
 (pretty long - 1.5 folding time 630 sec)
 $\Rightarrow \tau = 1.56 \text{ sec} \text{ (sec p 79)} \leq 1.8 \text{ sec}$

The system levelled itself off and went slightly subcritical
 at $\approx 4 \times 10^{-8}$ amps. Thermocouple readings were

Room - 70°F
 #1 - 106°F
 #2 - 109°F

Could temperature coefficient have done this?

Levelled at A 0.691 cm
 N 0.152 cm

Shut down 1600 PM, RTMS #2 - 10 R/hr

9/20/65

Starting temperatures Room - 71°F
 #1 - 102°F
 #2 - 108°F

Take a few multiplications for comparison with previous measurements.

S. S. Counter removed to test its neutronic worth on the measurements.

Assembly B-10

9/15/65

Ctr T-2

0.20

0.18

0.16

0.14

0.12

M-1

0.10

0.08

0.06

0.04

0.02

0.00

○ T-2 Actuator OUT
△ T-2 IN

5

4

3

2

1

0

Table Separation, cm

358-10^{1/2}
MADE IN U.S.A.

20 X 20 TO THE INCH
KEUFFEL & ESSER CO.

K&E

Position cm	T-1 cts/2 min	Eff.	n/sec $\times 10^{-6}$	M	T-2 cts/2 min	Eff	n/sec $\times 10^{-5}$	M
0.141	1238.3/3	7.5×10^6	91.72	5.70	11998/3	9×10^6	74.07	4.61
0.554	T/C's Room -	70 °F, #1 - 98 °F, #2 - 104 °F						
15.00 A								
0.141	151701/2	7.5×10^{-6}	1685.60	104.82	135-076/2	9×10^{-6}	1250.70	77.78
0.304	T/C's Room -	70 °F, #1 - 98 °F, #2 - 105 °F						
15.00 A								
0.141	357341/2	7.5×10^{-6}	3970.45	246.90	306133/2	9×10^{-6}	2834.55	176.27
0.204	T/C's Room -	71 °F, #1 - 99 °F, #2 - 106 °F						
15.00 A								

(Selsyn 0.145)

Set up with 0.152 H and took to critical on the actuator. Got ~900 sec period with actuator ~1.20 cm. Apparently it is not possible to locate the horizontal table with high accuracy from one day to the next because of drifts in the DVM values. Scrolled until 1.182 H at ~ 3×10^{-8} amps

Check worth of table motion

$$0.152 \text{ H}$$

$$\frac{0.149 \text{ H}}{0.003 \text{ cm}}$$

$$\Delta x = 0.003 \text{ cm} \approx \text{2-folding time } 111 \text{ sec}$$

$$\approx \text{period of } 160 \text{ sec}$$

$$\approx \frac{P}{2} = 7.6 \text{ sec}$$

Recheck int. with Geiger register at 0.15 H (DVM 0.154)

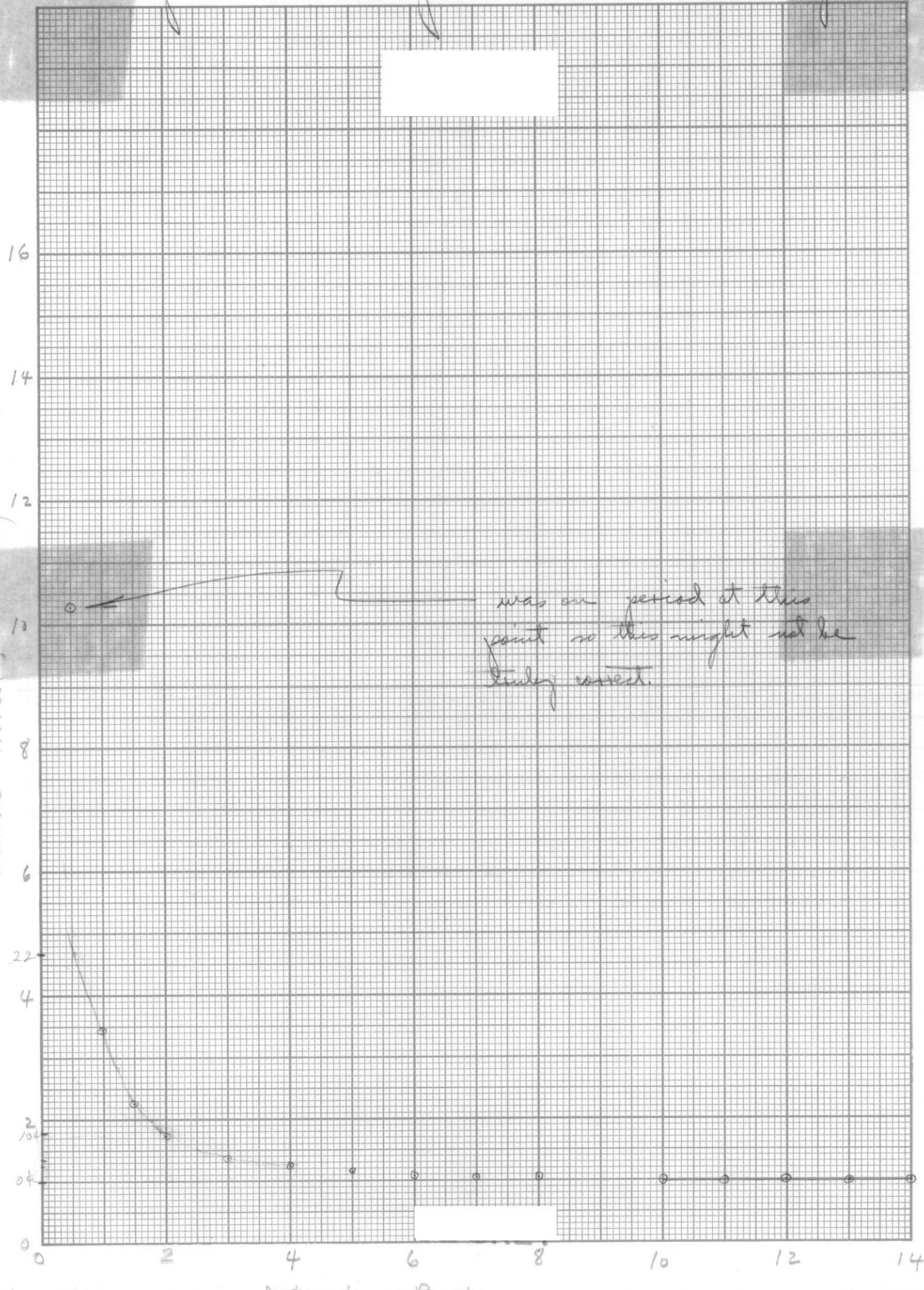
Ground level power at 0.681 A (2×10^{-8} amps)

Hence the S.S. counter seems to have no measurable neutron effect upon the array.

Horizontal table motion worth:

$$\Delta g / \Delta x = 0.076 / 0.003 \text{ cm} = 25 \text{ $/\text{cm}$}$$

Plot of relative worth of control actuators Assembly B-7



9/21/65

87

Made some adjustments on the linear pot. on the horizontal table. This reduced the hysteresis and greatly improved its action. Re-calibrated.

Starting temps

Room - 71°F # 1 - 97°F # 2 - 105°F

Position cm	T-1 cts	EFF.	η/sec $\times 10^{-5}$	M	T-2 cts	EFF	η/sec $\times 10^{-5}$	M
0.14V 9.55SH 15.00A	12761/3min T/C's Room - 71°F	7.5×10^{-6}	94.52	5.88	12759/3 #1 - 100°F	9×10^{-6}	79.01	4.91
					#2 - 105°F			

Start up with actuator at 2.00 cm

Ran my to power of 4.3×10^{-8} amps. Min. period with positions

$$\begin{aligned} H &= 0.166 \quad (0.15 \text{ Veder}) \\ A &= 0.289 \end{aligned}$$

2-folding line $142.5 \text{ sec} \approx 206 \text{ sec period} \approx 6 \text{ f}$

Levelled at above level $H = 0.166 \quad (0.15 \text{ Veder})$

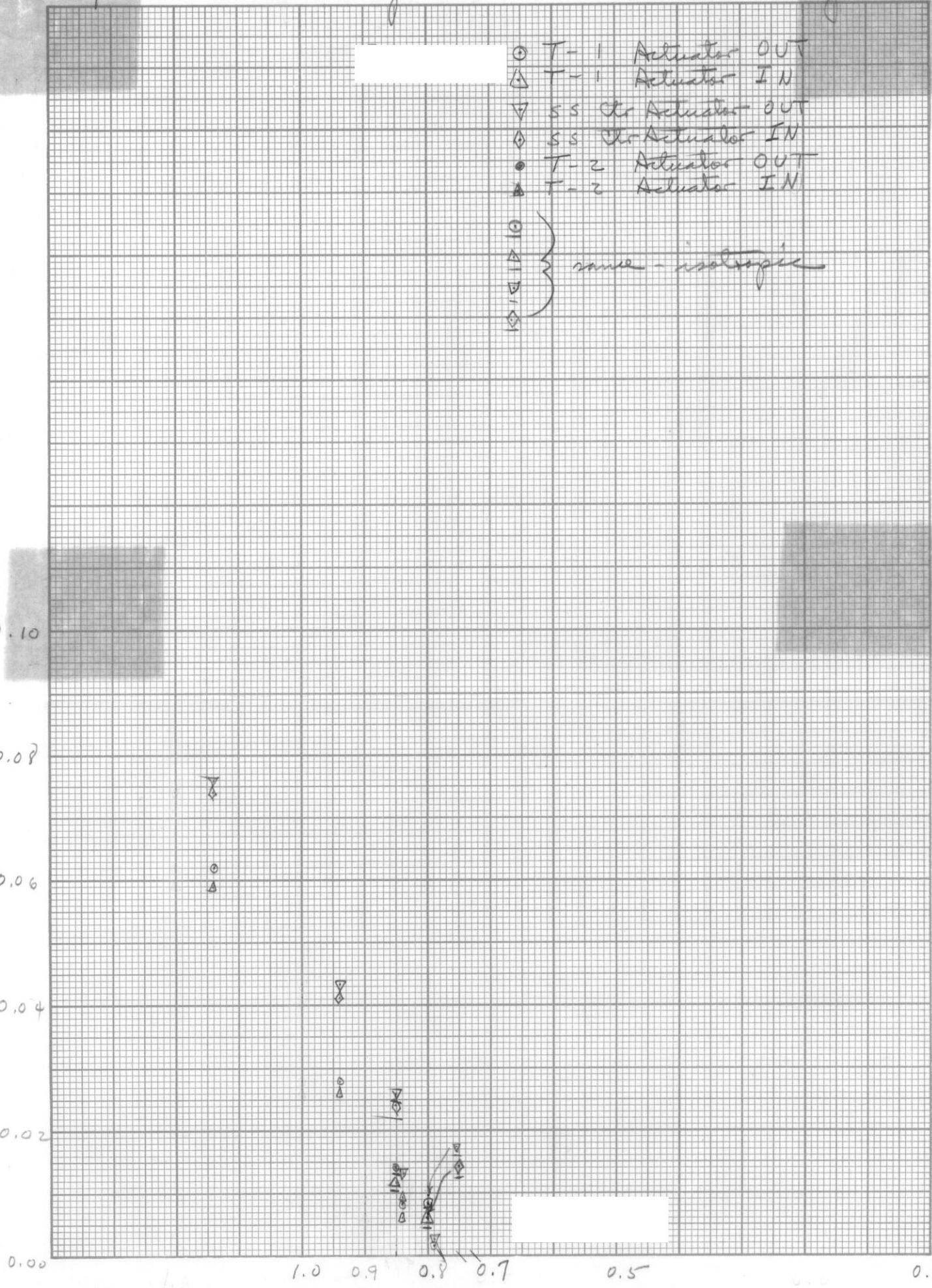
To maintain level $A = 0.429$ } $\Delta x = 0.067 \text{ cm}$
 $A \rightarrow 0.362$ } $\approx \$1.88$

T temps. at power

Room - 70°F # 1 - 102°F # 2 - 105°F

Temp of # 1 varied $\sim 2-3^{\circ}\text{F}$ during operation at power.

9/9/65 Bare 8-member Array Ctrs T-1 and SS (Larger Scale)



358-10^{1/2}
MADE IN U.S.A.

20 X 20 TO THE INCH
KEUFFEL & ESSER CO.

Counter T-1

Base 8-member Array

○ Activator OUT } Anisotropic
△ Activator IN }
□ same - isotropic

M⁻¹

○

0.10

35810½
MADE IN U.S.A.

20 X 20 TO THE INCH
KEUFFEL & ESSER CO.

K&E

○

○

○

○

○

0.14

0.12

0.10

0.08

0.06

0.04

0.02

0.00

2.0

1.0

0.0

Ave. Spacing, cm

Front

Front

Counts - T-2

Base 8-member Array

- Actuator OUT (Anisotropic)
- △ Actuator IN (Anisotropic)
- ◎ Actuator OUT (Isotropic)
- Actuator IN (Isotropic)



M^{-1}

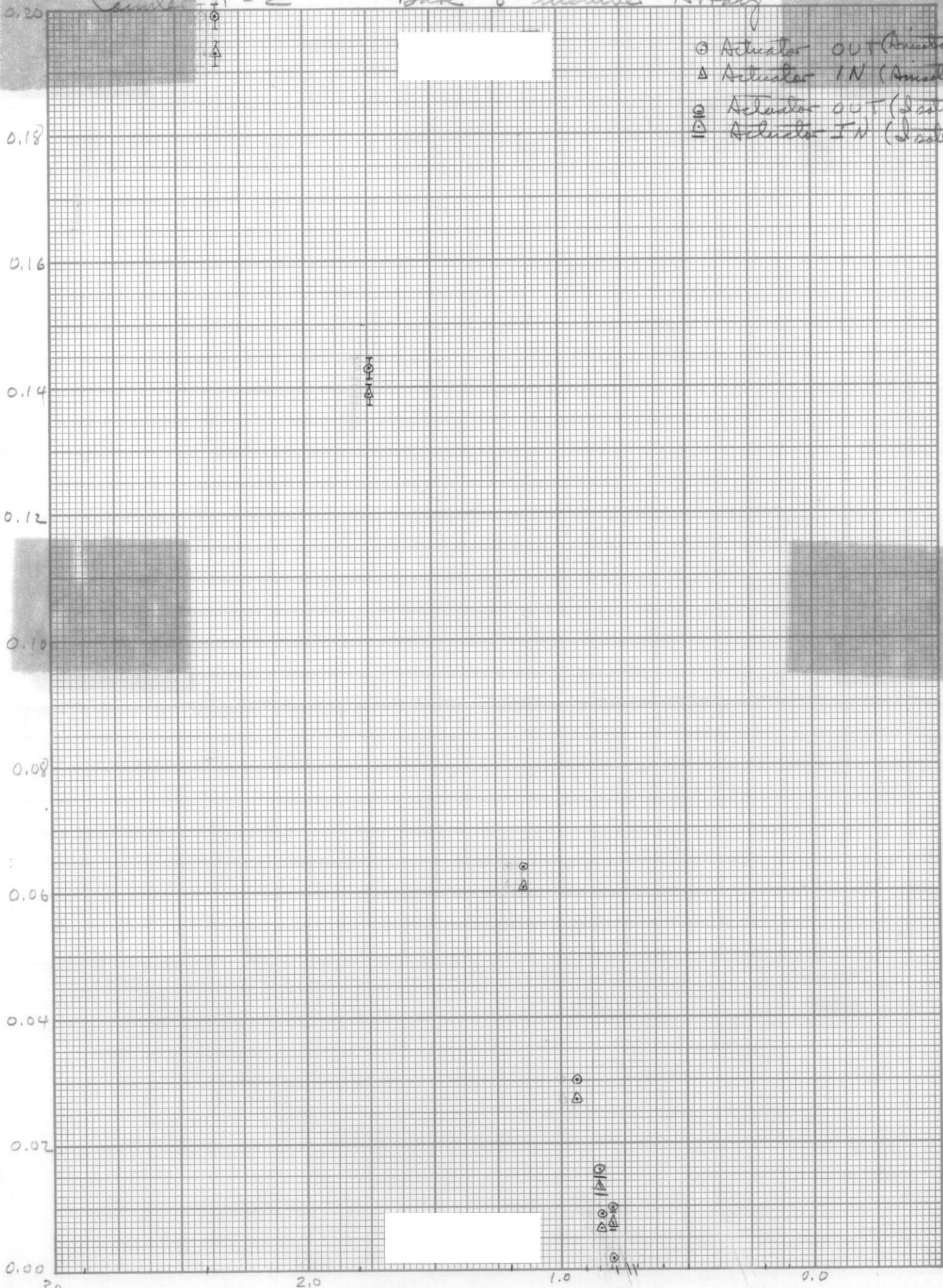


358-10½
MADE IN U.S.A.

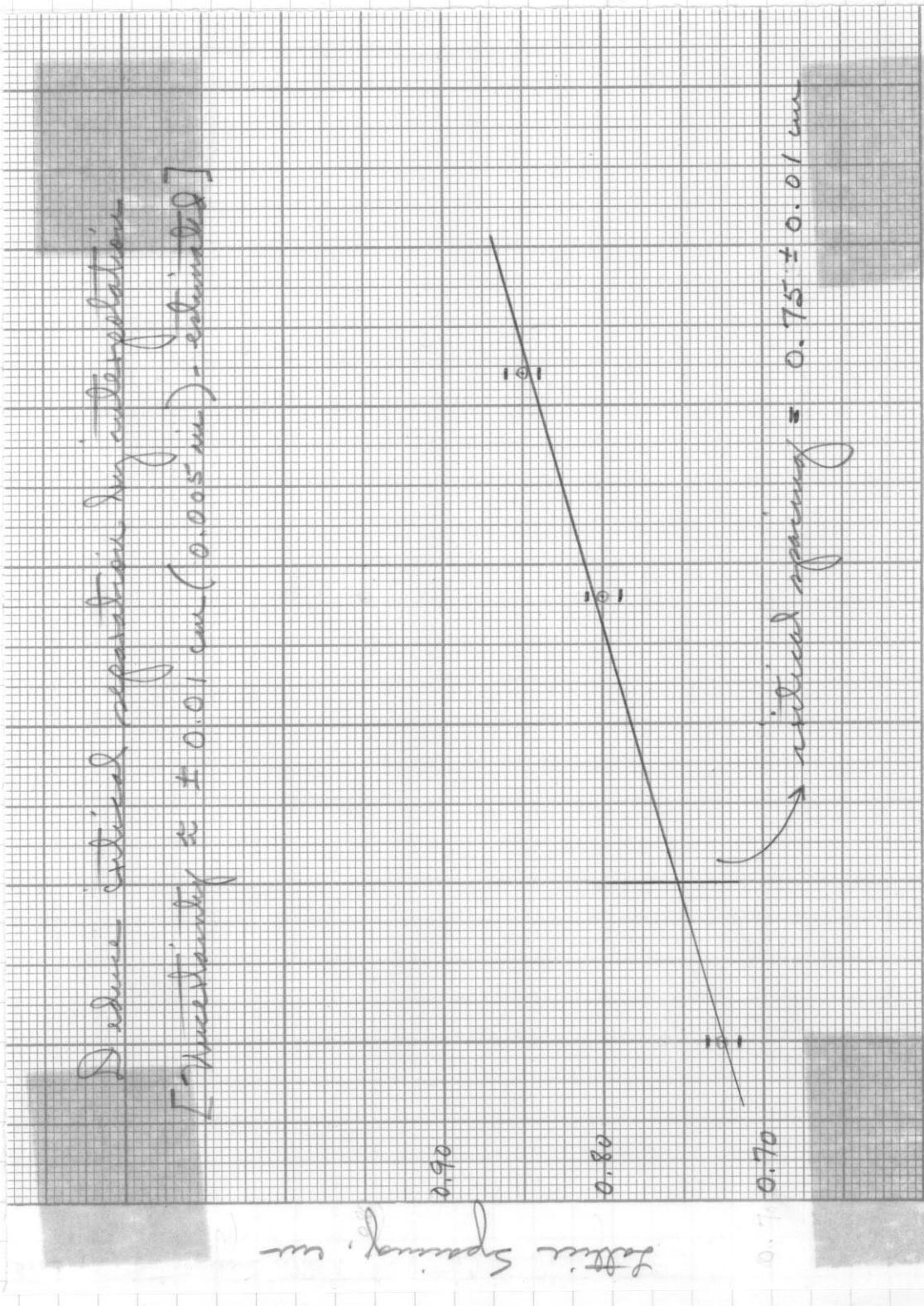
20 X 20 TO THE INCH

KEUFFEL & LESSER CO.

K&E



Sar. Spacing, cm



(Succeeding measurements will be recorded in Vol 2, which is not classified. The remainder of this notebook will be reserved for classified notes.)