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## 3.4. THE POISONING EFFECT OF COPPER LATTICES IN AQUEOUS SOLUTIONS OF ENRICHED URANYL OXYFLUORIDE

J. K. Fox L. W. Gilley

The use of metallic copper in the design of some uranium processing plant equipment has established a need for information on the effects, from a nuclear safety standpoint, of copper placed in or near uranium solutions. Accordingly, a series of experiments to measure the poisoning effect of lattices of copper tubes and rods on an aqueous solution of uranyl fluoride was performed.

The solution used in these experiments was 93.2% U<sup>235</sup>-enriched UO<sub>2</sub>F<sub>2</sub> in water, at a concentration of 0.4693 g of U<sup>235</sup> per cubic centimeter of solution, corresponding to an H:U<sup>235</sup> atomic ratio of 52.6. It was contained in a 10-in.-dia aluminum cylinder, which for most experiments was surrounded by a  $\frac{1}{4}$ -in.-thick copper shell, except for the top and bottom. With the exception of one case, the cylinder was reflected with water on the sides and bottom. In several experiments the copper tubes and rods were held in a stainless steel basket consisting of six <sup>3</sup>/<sub>2</sub>-in.-dia by 6ft-long rods equally spaced on a 9.5-in.-dia ring and attached to a perforated bottom plate. For most of the experiments, however, the copper was loaded directly into the containing vessel with edges in contact, forming a pseudo-triangular pattern. Using tubes having various diameters and wall thicknesses and placing small tubes inside larger tubes enabled the volume percentage of metal to be varied considerably.

The results of the experiments are given in Table 3.4.1, and typical curves showing the critical solution height as a function of the volume percentage of metal are plotted in Fig. 3.4.1. It can be seen that, for the case in which solution only was inside the cylinder, displacing a portion of the water reflector with the copper shell increased the critical solution height from 6.55 to 6.96 in. For the case in which the cylinder contained 27.7 vol % of copper, displacing a portion of the water reflector with the copper shell increased the solution critical height from 21.3 in. to 58.7 in. Inserting the stainless steel basket in the otherwise unpoisoned solution increased the critical height from 6.96 in. to 7.33 in., the copper



Fig. 3.4.1. Critical Height of a Reflected 10-in.-dia Aluminum Cylinder Containing a Copper-Poisoned Aqueous Solution of 93.2% U<sup>235</sup>-Enriched UO<sub>2</sub>F<sub>2</sub> as a Function of Copper Content.

Table 3.4.1. Critical Parameters of a 10-in-dia Aluminum Cylinder Containing an Aqueous Solution of 93.2% U<sup>235</sup>-Enriched UO<sub>2</sub>F<sub>2</sub> Poisoned with Copper or Aluminum Tubes or Rods

Solution concentration: 0.3195 g of U per g of solution; 0.4693 g of U<sup>235</sup> per cc of solution H:U<sup>235</sup> atomic ratio: 52.6 Solution specific gravity: 1.576

Number of Tubes or Rods	Tube or Rod			Critical Conditions							
	Dimensi Inside Diameter	ons (in.) Outside. Diameter	Metal Content (vol %)	Solution Height (in.)	<sup>Mass</sup> (kg of U <sup>235</sup> )	Description of Assembly					
	<u></u>			H <sub>o</sub> O Refle	tor Only	· · · · · · · · · · · · · · · · · · ·					
				6.55	3.96	Contained solution only					
		Conner Tub		a kin atra	Come Shall R						
Copper Tubes and Roas; 74-In-thick Copper Shell Plus H <sub>2</sub> U Reflector											
				6.96	4.21	Contained solution only					
12 1	1.933 1.272	2.375	23.9	14.2	6.53	Tubes uniformly distributed					
12 13	1.933 1.272	2.375 1.66	37.6	60.2 (NC) <sup>a</sup>		12 small tubes inside large tubes; one small tube outside					
12 2 2 17 18	1.933 1.368 0.822 0.495	2.375 1.66 1.05 0.675 0.25	30.8	35.2	14.7	2.375- and 1.66-in. tubes uniformly dis- tributed; smaller tubes successively placed in one another and uniformly distributed between large tubes					
12 3 3 8 15	1.933 1.368 0.822 0.495	2.375 1.66 1.05 0.675 0.25	30.3	59.3 (NC)		Essentially same as preceding except one 2.375-in. tube near center filled with successively smaller tubes					
26	1.272	1.66	29.5	31.3	13.3	Tubes uniformly distributed					
26 2	1.272 0.736	1.66	30.7	60.4	25.3	Small tubes inside large tubes near center					
26 3	1.272 0.736	1.66	31.2	45.0	18.7	Small tubes inside large tubes 120 <sup>0</sup> apart on outer edge					
26 4	1.272 0.736	1.66 1.05	31.8	50.8	20.9	Small tubes inside large tubes 90 <sup>0</sup> apart on outer edge					
26 4	1.272 0.736	1.66 1.05	31.8	50.5	20.8	Two small tubes inside large tubes; two small tubes outside; all on outer edge					
26	1.368	1.66	23.0	14.5	6.75	Tubes uniformly distributed					
26	1.368	1.66	23.0	58.4 (NC)		Tubes uniformly distributed; copper re- flector only					
26 6	1.368 0.736	1.66 1.05	27.4	24.2	10.8	Five small tubes inside large tubes near center; one small tube outside					
26 10	1.368 0.736	1.66 1.05	28.7	56.2	24.2	Small tubes inside large tubes near center					

Number of Tubes or Rods	Tube or Rod		Metal Content	Critical Conditions							
	Dimensions (in.)			Solution Height	Mass	Description of Assembly					
	Diameter	Diameter	(vol %)	(in.)	$(kg of U^{233})$						
Copper Tubes and Rods; $\frac{1}{4}$ -in-thick Copper Shell Plus H <sub>2</sub> O Reflector											
26 16	1.368 0.736	1.66 1.05	32.1	30.2	12.4	Small tubes inside large tubes near outer edge					
26 19	1.368 0.736	1.66 1.05	33.7	60 <sup>b</sup>	24.1	Small tubes inside large tubes around outer edge					
Copper Tubes Contained in Stainless Steel Basket; $^{c}$ $\frac{1}{4}$ -in,-thick Copper Shell Plus H <sub>2</sub> O Reflector											
				7.33	4.69	Contained only stainless steel basket plus solution					
60	0.822	1.05	25.6	22.2	9.98	Tubes uniformly distributed					
60 10	0.822 0.495	1.05 0.675	27.7	58.7	25.7	Ten small tubes inside large tubes near center					
Copper Tubes Contained in Stainless Steel Basket; <sup>C</sup> H <sub>2</sub> O Reflector Only											
60	0.822	1.05	25.6	15.5	6.97	- Tubes uniformly distributed					
60 7	0.822 0.495	1.05 0.675	27.1	19.2	8.46	Seven small tubes inside large tubes near center					
60 10	0.822 0.495	1.05 0.675	27.7	21.3	9.31	Ten small tubes inside large tubes near center					
4-inOD Copper Rod Plus Tubes Held in Stainless Steel Basket: <sup>C 1</sup> -in. Copper Plus H <sub>2</sub> O Reflector											
1		4.0	16.0	11.9	6.39	Single rod in center					
1 2	1.933	4.0 2.375 }	19.8	14.0	6.79	Two tubes adjacent to copper rod on adjacent sides					
1 4	1.933	4.0 2.375 }	23.6	18.1	8.36	Small tubes placed around center rod					
1 6	1.933	4.0 2.375 }	27.4	29.8	15.6	Small tubes placed around center rod					
1		4.0				Small tubes placed around center rod					
6	1.933	2.375 }	29.7	60 (NC)							
2	1.272	1.66 J									
Aluminum Tubes; $\frac{1}{4}$ -inthick Copper Shell Plus H <sub>2</sub> O Reflector											
7 9	2.062 1.590	2.375) 1.875	18.7	9.88	4.86	Tubes uniformly distributed					
7 12	2.062 1.590	2.375 ) 1.875 )	21.7	11.3	5.35	Tubes uniformly distributed					

Table 3.4.1 (continued)

<sup>a</sup>NC = not critical.

<sup>b</sup>This assembly was not critical, but the monitoring instruments indicated that removal of one small rod would have been more than sufficient to make the assembly critical.

<sup>C</sup>The calculations of critical volumes in these assemblies include the volume occupied by the basket; hence the volumes recorded are slightly high.

shell displacing part of the water reflector in both cases.

In some experiments the copper placement was varied in steps radially from the center. It was observed that the metal was more effective in positions near the center, a 4-in.-dia rod at the center having the greatest effect. It was also observed that for a given volume fraction the smaller-diameter tubes had a greater effect than the larger ones. An indication of the relative effects of displacement of solution and poisoning by the copper was obtained by substituting aluminum tubes for copper in two experiments, since aluminum has a very low absorption cross section. Comparison of aluminum data with corresponding copper data where the tube sizes and distributions are similar indicates that displacement of solution is more important than the neutron absorption effect. This is clearly seen by comparison of the curves in Fig. 3.4.1.